NRL Memorandum Report 3611 AD A 0 50 0 5.4 **Data Compendium for Atmospheric Laser Propagation Studies** Conducted at Cape Canaveral, Florida February-May 1977, A/GUTTMAN, Editor. T. H. Cosden, J. A. Curcio, J. A. Dowling D. H. Garcia, C. O. Gott, A. Guttman, S. T. Hanley, K. M. Haught, R. F. HORTON, G. L. TRUSTY, and W. L. AGAMBAR Optical Radiation Branch 14/NRL-MR-3611 Optical Sciences Division

NAVAL RESEARCH L. BORATORY Washington, D.C.

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NRL Memorandum Report 3611	
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PROPAGATION STUDIES CONDUCTED AT CAPE	NRL problem.
CANAVERAL, FLORIDA, FEBRUARY - MAY 1977	6 PERFORMING ORG REPORT NUMBER
7 AUTHOR :	CONTRACT OR GRANT NUMBERIO
A. Guttman, Editor, T.H. Cosden, J.A. Curcio, J.A. D	- · · · · · · · · · · · · · · · · · · ·
D.H. Garcia, C.O. Gott, A. Guttman, S.T. Hanley, K.I.	M. Haught,
R.F. Horton, G.L. Trusty, and W.L. Agambar	
9 PERFORMING ORGANIZATION NAME AND ADDRESS	10 PROGRAM ELEMENT PROJECT TASK AREA & WORK UNIT NUMBERS
Naval Research Laboratory	NRL Problem R05
Washington, D.C. 20375	Project 405-003-173-1-SRSL
Department of the Navy	12 REPORT LATE
Naval Sea Systems Command (PM-22/PMS-405)	September 1977
Washington, D.C. 20362	13 NUMBER OF PAGES
14 MONITORING AGENCY NAME & APPRESHIE ditterant from Contr.	1
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20 Abstract (Continued)

For Koschmieder type measurements of the concrast of distant (argets. Results of extensive monitoring of the HDO path concentration with a Gas Filter Correlation Spectrometer (GFCs) show an abundance ratio significantly lower than the literature value of 0.03%.

Results of in-situ meteorological measurements and aerosol particle size distribution samplings are also reported. \Box

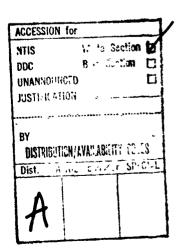
FOREWORD

The data contained in this report are preliminary and presented here in the interest of rapid dissemination. Further refinements in data processing may lead to minor revisions.

For detailed discussion on particular aspects of the material contained herein the following personnel may be consulted;

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Gas Filter Correlation Spectrometry	s.	Т.	H a nley
Basic Meteorological Data	D.	н.	Garcia
Aerosol Particle Spectrometry	G.	L.	Trusty

Dr. J. A. Dowling was Project Officer and responsible for overail coordination of this project.



ABSTRACT

Atmospheric transmission measurements were carried out at Cape Canaveral Air Force Station during the spring of 1977 by means of the NkL Infrared Mobile Optical Radiation Laboratory (IMORL). Reduced data resulting from this effort are presented in this report for five laser wavelength regions (HeNe, Nd-YAG, DF, CO, CO₂). Typical high-resolution ($\Delta\omega$ =.08 cm⁻¹) transmission spectra included in this report were derived on the basis of Fourier transform spectroscopy. An extensive set of aerosol scattering coefficient data is reported for 15 visible wavelengths and is based on Koschmieder type measurements of contrast of distant targets. Results of extensive monitoring of HDO path concentration with a Gas Filter Correlation Spectrometer (GFCS) show an abundance ratio significantly lower than is commonly reported in the literature. Results of in-situ meteorological measurements and aerosol particle size distribution samplings are also reported.

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DATA COMPENDIUM FOR ATMOSPHERIC LASER PROPAGATION STUDIES CONDUCTED AT CAPE CANAVERAL, FLORIDA, FEBRUARY-MAY 1977

1. INTRODUCTION

During the months of February through May 1977, the Infrared Mobile Optical Radiation Lab (IMORL) of NRL was operated at the Cape Canaveral Air Force Station (CCAFS) in Florida to conduct an extensive series of atmospheric transmission experiments. A principal objective of these experiments was to obtain precisely calibrated high-resolution atmospheric transmission spectra in the 3-5 μm and 8-14 μm atmospheric windows suitable for rigorous comparisons to computer models. Absolute transmission calibration of the FTS spectra is obtained by means of extinction measurements at several laser frequencies performed with minimal time offset from the FTS measurements. Emission spectra of the laser sources operated multi-line is used to generate accurate frequency calibrations of the atmospheric transmission spectra using the well known positions of the several laser lines used in the experiments.

A secondary objective of the CCAFS experiments was the evaluation of the effects of absolute humidity variations and the influence of aerosol scattering on the atmospheric extinction of several infrared laser lines in the above spectral regions.

A detailed description of the IMORL instrumentation may be found in Ref. 1. Experiments were conducted over a 5.1-km. overwater path, shown in Fig. 3.1 as Path 3. Atmospheric extinction and spectroscopic data were collected with the following apparatus:

- (1) HeNe,Nd-YAG, DF, CO, and ${\rm CO}_2$ lasers
- (2) Fourier Transform Spectrometer (FTS)
- (3) Gas Filtc: Correlation Spectrometer (GFCS)
- (4) Bandpass filtered telephotometer operating at 14 wavelengths and optical pyrometer at two wavelengths
- (5) Aerosol particle spectrometer
- (6) Nephelometer operating at three wavelengths
- (7) Basic meteorological measurement apparatus

New additions to the IMORL system which were used extensively for the first time include a short wavelength CO laser, the FTS, the GFCS and the filtered telephotometer.

Presented in this report are the data gathered during the three month period with all the above instrumentation except the nephelometer. Data processing for the latter was not completed in time to be included here. A summary of laser extinction, FTS, GFCS, absolute humidity and visibility data is given in Table 1.1.

Note: Manuscript submitted September 8, 1977.

The laser beam extinction data are presented in Section 2. Section 3 contains a complete listing of all visible extinction data derived on the basis of telephotometric and pyrometric contrast measurements. Samples of the high resolution atmospheric absorption spectra obtained with the SMI are shown graphically in Section 4. Results of the GFCS measurement yielding HDO/H₂O abundance ratios are contained in Section 5, while Section 6 includes selected data from the on-site meteorological stations, including aerosol spectrometer measurements.

It should be noted that all times, unless otherwise noted, refer to local civil time, which was EST for the months of Feb-April and EDT for May.

2. LASER EXTINCTION MEASUREMENT DATA

This section contains data from line-by-line laser extinction measurements made at Cape Canaveral Air Force Station in the spring of 1977. Transmissions were measured for helium-neon, neodymium-YAG, deuterium fluoride, carbon monoxide, and carbon dioxide laser sources along a 5.1-km overwater path from February through May of 1977. An elaborate scheme has been worked out to correct for short- and long-term drifts to achieve overall accuracies which are typically better than 5%. A detailed discussion of the measurement procedure can be found in the paper by Dowling et al.

The columns appearing in Tables 2.0 to 2.4 include data given as day, month, and year. The months are Jesignated by a single letter with F, M, A, and Y corresponding to February, March, April and May respectively. The time is given on a 24-hour clock. "Run Code" denotes short-path normalization measurements by 0, 1, 2, 7, 8, or 9, long-path transmission by 3. 4, 5, or 6. The short-path normalizations are used for computer reduction and do not appear on the final tables. Line ID denotes a particular line of given laser source. A six digit alpha numeric code for line ID was used to designate a particular laser operating line and in some cases the detector used for the measurements according to the following scheme:

LASER CODE	LINE ID	LASER/LINE	(µm)	DETECTOR
0	POO-SI	H eNe	0.6328	Si diode
1	P11 - SI	Nd-YAG	1.06	Si diode
1	P11-IN	Nd-YAG	1.06	InSb diode (77K)
3	P02-08	DF/(2 → 1 P ₈ line)	3.8007	InSb diode (77K)
4	P05-09	CO/(5→4 P ₉ line)	4.9923	InSb diode (77K)
5	P10-20	$CO_2/00^{\circ}1 \rightarrow 10^{\circ}0$ band $(P_{20} \text{ line})$	10.5910	GeAu PC (77K)
5	RO2-20	$\frac{\text{CO}_2/00^{\circ}_{1} \rightarrow 02^{\circ}_{0} \text{ band}}{(\text{R}_{20} \text{ line})}$	9.2714	GeAu PC (77K)

"Mob" and "Stat Gain" refer to precision gain settings used on detector preamplifiers for a single measurement. "Trans" is the actual transmission over the 5.1-km path corrected for detector efficiency and optical-train transmission. "Ex Coef." is the corresponding extinction coefficient for the measured transmission at a single line and is expressed in units of km⁻¹. The optical-train efficiency is treated as a linear variable between two bracketing zero-path calibrations. For He-Ne and Nd-YAG, a single table summarizes all measurements in each case.

For DF, CO, and ${\rm CO}_2$, one table per day is used due to the large number of individual lines involved.

3. AEROSOL EXCTINCTION MEASUREMENTS

3.1 SPECTROPHOTOMETRIC DATA

Contrast reduction experiments based on the Koschmieder theory were performed along the three paths shown in Fig. 3.1. Path 3, which is identical with that used for the laser beam experiments. Path 2, with a range of 2.57km, is nearly parallel to the beach with a portion of it running over water but displaced not more than about 100 m from the shore. The short path, No. 1, has a length of 1.28 km and runs entirely over land, with a maximum perpendicular distance of about 100 m inland from the shore. As may be seen from the geometry these three paths represent a convenient means for probing gradients perpendicular to the shore. The light-measuring apparatus was placed at the convergence of the three paths, in close proximity to the laser receiving station situated on the beach in a large semitrailer van. Passive "black" targets defined the termination points at the far ends of the paths.

For any particular path, of length R, an apparent contrast ratio, $\boldsymbol{C}_{\boldsymbol{R}}$, is defined such that

$$C_{R} = \frac{N_{h} - N_{b}}{N_{h}} = 1 - \frac{\int_{0}^{\infty} N(r) dr}{\int_{0}^{\infty} N(r) dr},$$
 (3-1)

where N_b and N_h represent the apparent radiance of the black target at the end of the path, and the radiance of the horizon sky adjacent to the target, respectively. For daylight operation in the visible region of the spectrum these radiances represent predominantly scattered solar radiation. Thus the radiance integrand, N(r), in Eq. (3.1) refers to the total volume scattering by atmospheric particles into the observation direction resulting from illumination of the volume in all directions.

If one neglects the effects of earth's curvature and assumes homogeneity of scatterers and uniformity of illumination along the effective range of the path, the well-known Koschmieder analysis predicts an exponential decay of \mathbf{C}_{R} with range, i.e.,

$$C_{R}(\lambda) = e^{-\sigma} \lambda^{R}$$
 , (2)

where σ_{λ} refers to the monochromatic scattering coefficient at wavelength $^{\lambda}\lambda$, and the contrast ratio appears as a wavelength dependent function.

The quantity C_R was measured with a spectrally filtered telephotometer. Fourteen wavelengths were defined by bandpass interference filters which were used in sequence to observe black targets along the three paths shown in Fig. 3.1.

The resulting data are presented in Table 3.1 and shown graphically in Figs. 3.2, 3.3 and 2.4.

Fig. 3.5 shows the effect of wind speed on the nature of the spectra and on the gradients across the shore line.

3.2 PYROMETRIC DATA

The attenuation coefficient at 0.5568 and 0.6500 μm was determined visually by means of a telepyrometer. This is an optical pyrometer which has been modified by the addition of a telephoto lens. The attenuation coefficient was determined by measuring the radiance of a suitable black target and also the radiance of the adjacent horizon sky. These radiances are then applied to the Koschmieder relationship, which relates luminance to attenuation (see Sec. 3.1). In this simplified form the target is black and the measurement is made in a spectral region of minimal absorption, so that the observed attenuation is caused by molecular and aerosol scattering. In practice the apparent spectral brightness temperature of the target and horizon sky is determined by the optical pyrometer. From the known blackbody spectral radiance as a function of temperature, the attenuation coefficient is determined from the Koschmieder relationship, Equation (3-1). Four optical path lengths, of 3.10, 4.61, 5.08 and 7.47 km were used for these measurements. A small structure located near the laser transmitter site, Figure 3.1 was used for the 3.1 and 5.08 km paths with the pyrometer located near the aerosol sampling station and receiver site respectively. For the 4.61 and 7.47 km paths tree lines located near the shore line served as black targets with the pyrometer located at the laser transmitter site.

Table 3.2 gives the complete set of data in terms of three basic parameters, namely, path transmittance, extinction coefficient, and meteorological range (VIS.).

4. HIGH-RESOLUTION FTS MEASUREMENTS

The high-resolution atmospheric transmission measurement were made with an IDAC Model 1000 Fourier transform interferometer. Spectrometer (FTS) system. A description of the FTS system and of its installation in the IMORL receiver trailer appears elsewerel and will not be repeated here.

For the 1977 Cape Canaveral experiments the interferometer was operated in two distinct modes, depending upon the spectral region being investigated.

For work in the 3 µm to 5 µm atmospheric window, the interferometer was configured with a CaF₂ beamsplitter and an InSb deter or. Inteferograms of a graybody source in the IMORL transmitter traiter (5 km distant) were sampled at 128 K equally spaced points over a total optical retardation of 8 cm. To reduce noise levels in the resulting computed spectra, 100 interferometer scans were typically co-added prior to calculating the Fourier transform. The sampling process generally required about fifteen minutes.

For work in the 10 µm region, the FTS system was used with a KBr beamsplitter and a HgCdTe detector. The 8 cm optical retardation was retained, but the sampling was reduced to 64 K (equally spaced) points. Because the background radiation in this region is proportionately larger, separate "no-source" scans were also recorded. These reference interferograms provide data on the spectral distribution of the atmospheric background radiation, which must be separated from the graybody spectra before attempting an absolute transmission normalization. (To date, initial efforts to affect this separation by simply differencing the two types of interferogram prior to computing the Fourier transform have not proved satisfactory.)

Examples of spectra obtained with the FTS system are presented in Figures 4.1, 4.2, and 4.3. These spectra (chosen to cover a wide range of water vapor pressures) also incorporate preliminary transmission normalizations, based on the laser absolute transmission measurements. Care must be exercised when interpreting the "flat top" features seen in these spectra in regions of low transmission. The current software used by the FTS system does not correctly compute the ratio of a long-path spectrum to a short-path background spectrum when both the numerator and the denominator are small. In such cases, however, the atmospheric transmission at five kilometers is small (less chan 5%). A description of the laser measurements is presented in Section 2 of this report, and the techniques used to obtain a preliminary normalization have been presented in several earlier reports.

Finally, development is currently nearing completion of a new series of computer programs designed to standardize the transmission normalization of sampled atmospheric spectra. These programs directly

process spectra from the magnetic tapes written by the FTS data aystem, and produce both graphical and digital magnetic tape output. It is expected the remainder of the high-resolution, laser-calibrated spectra from the Florida experiments should be available within two months.

5. GAS FILTER CORRELATION SPECTROMETER MEASUREMENTS

The atmospheric abundance of the molecular species HDO was measured with a gas filter correlation spectrometer (GFCS) during field measurements at the Patuxent Naval Air Station in November of 1976 and at Cape Canaveral Air Force Station (CCAFS) in the spring of 1977. This device is described in Jetail in reference (1). Data taken during the CCAFS experiment are plotted in Figures 5.1-5.23. Each plot presents a complete set of data taken during one day. HDO abundances determined by the GFCS are indicated by the symbol G. Also shown in Figures 5.1-5.23 are HDO abundances determined from local dew-point measurements using the widely accepted value of 0.03% for the HDO/H2O abundance ratio and the measured air temperature. Dewpoint measurements were performed at the transmitter, receiver and mid-point locations along the measurement path shown in Figure 3.1. The HDO abundances (expressed as molecules/cm/cm) derived from them are indicated by the symbols T, R, and M respectively in Figures 5.1-5.23.

Earlier GFCS data taken during the Patuxent NAS experiment are plotted in Figure 5.24 as water vapor partial pressure (using the 0.03% abundance ratio) against local time for several days.

METEOROLOGICAL MEASUREMENTS

6.1 BASIC METEOROLOGICAL DATA

Three independent systems were used during the atmospheric transmission experiments to monitor and record the meteorological conditions at the two ends of the 5.1-km path and at a point approximately midway. One system was located in the office trailer van next to the transmitter van; another identical system was located in the mobile receiver trailer van and was operational during long-path measurements. A third, similar system was situated in the mobile meteorological van at the path halfway point.

These systems include the following meteorological sensors: an automatically balancing EG&G Model 110S-M dew-point hygrometer to measure atmospheric temperature and dew point; a Yellow Springs Instruments Company Model 2014 barometric-pressure transducer; an Eppley Laboratory No. 8-48 Black and White Pyranometer to measure global (total sun and sky) radiation; a Thornthwaite Associates Model 912 sensitive-cup anemometer to measure wind speed at the path ends; a Young Gill Model 35003 propeller Vane to measure wind speed and horizontal wind direction at the midpoint; and a Young bivane to measure horizontal and vertical wind direction at each path end.

Analog voltages from each meteorological sensor are processed by a Monitor Labs 7200 data-acquisition system at each path end and by a Particle Measuring Systems data-acquisition system at the midpoint location. The outputs are digitally recorded on magnetic tape for subsequent reduction at NRL.

Table 6.1.1 lists the available meteorological data for the period 23 February through 25 May 1977 at the three monitoring sites: transmitter T, mobile met van M, and receiver/spectrometer, S. Air temperature AT is in degrees Celsius; the partial pressure of water vapor PPH₂O is in torr; barometeric pressure BP is in millibars; global/solar radiation SR is in watts per square meter; wind speed WS is in meters per second; and horizontal wind direction WDH is in degrees clockwise from magnetic north. Blank spaces in this table indicate unavailability of data for that time for a particular sensor due to operational difficulties in the field; lack of an entry for any system at the approximate half-hour mark indicates nonexistence of data at that time or failure in processing system tape for that day or time of day. Each entry in this table is a 6-minute average terminating at the time indicated.

Figure 6.1.1 shows an example of the variation in air temperature and partial pressure of water vapor observed at the three monitoring sites during a particular day (15 March 1977).

6.2 PARTICLE SPECTROMETRY

The Laser/Aerosol Interaction Section of the Optical Radiation Branch provided, for the first three months of the 1977 Florida experiment, measurements of aerosol distributions and readings from one set of meteorological instruments. The data from the aerosol measurements are provided here in Table 6.2.1. The meteorological measurements were presented above in Section 6.1 (location M).

The equipment used for obtaining the aerosol size distributions included two optical particle spectrometer probes and a buffer memory manufactured by Particle Measuring Systems. The Active Scattering Aerosol Spectrometer Probe (ASASP) monitors particles from 0.1 μm radius to 2.0 μm radius with a sample volume flow rate of 0.11 cm $^3/\rm{sec}$. The High Volume Classical Aerosol Spectrometer Probe (HVCASP) monitors particles from 1.0 μm to 15 μm radius with a sample volume flow rate of 49 cm $^3/\rm{sec}$.

Sampling occurs on a one-second basis in the system as configured. These data are recorded on a 9-track computer compatible magnetic tape which is later reduced to the desired averaging times. For the work in Florida six-minute averages were chosen as giving acceptable counting statistics while minimizing the time-slew which might degrade the resolution of any major, abrupt aerosol density fluctuations.

For the purposes of this compendium, the resultant six-minute averages are given only on the half hour as shown in Table 6.2.1. Presented there are aerosol size distributions in the form of particle density $(\Delta N/\Delta R)$ as a function of particle radius (R). The density is found from the average number of counts per second in a bin divided by the sample volume flow rate divided by the width of the sampling bin (ΔR) which has its center at radius R. The entries for the first seven bin locations are obtained from the ASASP; the remaining fifteen are obtained from the HVCASP.

The relatively large gap between the bins with centers at 0.33 μm and 1.22 μm is the result of an inherent double-valued response function in the ASASP which arises because a single frequency light (a HeNe laser) i, used as the illuminating source. Because the simple approach as Jescribed above for obtaining $\Delta N/\Delta R$ gives structure which is nonexistant in the actual distribution in that particular region, the results obtained from those bins have been omitted.

The extinction coefficients which are calculated from these distributions will be presented in a later report with a detailed analysis.

REFERENCES

- 1. J. A. Dowling, R. F. Horton, G. L. Trusty, T. H. Cosden, K. M. Haught, J. A. Curcio, C. O. Gott, S. T. Hanley, and P. B. Ulrich, "Atmospheric Transmission Measurement and Field Test Plan," NRI. Report 8059, (September 77).
- 2. T. H. Cosden, J. A. Curcio, J. A. Dowling, C. O. Gott, D. H. Garcia, S. T. Hanley, K. M. Haught, R. F. Horton, and G. L. Trusty, "Atmospheric Transmission Measurements Program Report for FY7T: 1 July 1 October 1976," NRL Report (August 1977).
- 3. K. M. Haught and J. A. Dowling, "Laser-Calibrated High-Resolution Atmospheric Transmission Measurements," OSA/IEEE Conference on Laser Engineering and Applications, Washington, D. C. (June 1977).
- 4. K. M. Haught and J. A. Dowling, "High-Resolution Atmospheric Absorption Spectra from 3 μm to 5 μm ," Thirty-Second Symposium on Molecular Spectroscopy, Columbus, Ohio (June 1977).

TABLE 1,1, 1977 CCAFS EXPERIMENT SUMMARY

 	+	LASEK	×		FTS		CFCS	7:	XFT
Pathlength (m)	Time	Lasers	# Lines Measured	Time	FTS Spectral Interval (cm ⁻¹)	Code*	GFCS	ppH ₂ O (Torr)	visibility (km)
20	1430-1610	°2	. 09	ł	1	1	;	13.6	24.3
=	1420-1830	HeNe, DF, CO ₂	\$9	1530	0-7800	211	:	12.8	11.9
=	1	ł	1	1840	1800-3200	111	;	=	=
=	1030-1615	=	7.5	ł	1	ł	1	14.6	19.0
=	1530-1800	=	11	1610	1600-3200	211	1	5.8	42.9
ž	ı	ł	;	1700	1800-3200	111	1	å	r
÷	ì	;	;	1820	1800-3200	111	;	2	=
5080	0950-1450	HeNe, CO_2	67	1240	1800-3200	111	×	7 0	35.0
=	1130-1430	DF	77	1250	1800-3200	111	>:	13.1	20.0
=	i	;	;	1250	0-7800	111	×	;	=
=	1045-1250	HeNe, \mathbf{CO}_2	21	ŀ	1	ŀ	×	16.0	20.0
=	0930-1600	:	68	1210	800-3200	112	×	9.2	19.5
=		i	;	1225	800-3200	7	×	z	=
=		ł	;	1300	0-7600	=	×	•	=
:	1000-1618	HeNe, DF, CO ₂	76	1310	1800-3200	111	×	11.7	14.0
=	;	:	i	1335	1800-3200	111	×	=	:
:	1150-1540	reNe, CO	87	1050	1800-3200	111	×	15.0	10.0
=	1125-1700	=	81	1300	0-3900	132	×	16.0	18.0
:	1025-1530	:	70	1155- 1600	+	132	*	16.5	21.0

TABLE 1.1 , 1977 CCAFS EXPERIMENT SUPMARY

			LASER	~		FTS		GFCS	MET	ī
Date	Pathlength (m)	Time	Lasers	# Lines Measured	Tine	FTS Spectral Interval (cm ⁻¹)	Code*	GFCS	ррН ₂ 0 (Тогг)	visibility (km)
3-14	E	1000-1715	=	156	1320- 1415	+	132	×	7.0	24.5
3-15	2	0830-1430	z	70	1110-	+	032	×	12.5	25.0
3-16	20	1340-1450	:	41	1520	+	232	;	16.6	19.0
3-17	=	1020-1450	:	73	;	1	1	:	:	:
2ND SESSION	×									
3-29	:	;	i	;	1545	800-3200	132	1	15.0	30.5
	z	;	1	;	1545	0-3900	132	;	Ξ	•
	=	ŀ	1	:	1545	0-1900	132	ŧ	ı	=
30	Ė	1000-1630	Hene, DF, CO ₂	138	1305	1800-3200	111	;	17.5	25.0
	=		:		1320	1800-6600	111	1	:	I
31	5080	1400-1600	HeNe, DF	27	1245	1800-6600	111	×	18.0	30.0
	=	ŀ	;	1	1245	0-7800	111	×	=	=
7-7	=	1000-1600	π. νε. υΓ. co, co,	88 80	1310	1800-3200	111	×	18.0	20.0
	ŧ			1	1330	1800-3200	111	×	:	=
	=				1635	800-3200	132	×	:	=
7	ŧ	0950-1645	HeNe, YAG, DF, CO ₂	138	1345	800-3200	132	×	18.5	29.8

TABLE 1.1. 1977 CCAFS EXPERIMENT SUPMARY

			LASER	,		FTS		SECS	Law	F
Date	Pathlength (m)	Time	Lasers	# Lines Measured	Time	FTS Spectral Interval (cm ⁻¹)	Code*	GFCS	ppH ₂ 0 (Torr)	visibility (km)
4-2	.	ł	;	;	1345	0-3900	132	×	=	H
	5080	1	!	!	1400	800-3200	132	×	18.5	29.8
	=	ŀ	ł	1	1400	0-3900	132	×	=	Ξ
7-7	ŧ	0915-1630	HeNe,YAG, DF, CO ₂	180	1235	800-3200	132	×	18.0	21.0
	:	1	1	ł	1255	800-1400	132	×	=	£
		;	ŀ	;	1310	800-1600	032	×	=	2
		ŀ	;	1	1310	0~3900	032	×	ż	z
4-5	=	1045-1545	HeNe, YAG, DF, CO	22	1350- 1425	+	132	×	10.5	50.0
4-6	90	0930-1650	=	129	1230	800-3200	132	ł	7.0	60.09
	:	į	ŀ	ŀ	1245	800-3200	132	ŀ	2	=
4-7	=	0940-1430	HeNe,YAG, DF, CO ₂	66	1245	1800-3700	111	ŀ	6.8	53.0
		ł		ł					=	=
3RD SESSION	*									
5-13	20	1500-1700	DF, CO	6	;	ł	1	;	;	1
14	=	1030-1745	HeNe,YAG, DF,CO,CO ₂	130	1140	1800-3200	311	ł	12.8	1
	:	ţ	;	;	1240	1800-6600	311	i	12.4	1
	=	ł	;	1	1300	1800-3200	311	ł	:	;

TABLE 1.1. 1977 CCAFS EXPERIMENT SUMMARY

2400 Time Lasers 7 Lines Time Greening Location Control Lines Time Control Lines				LASER	<u>e</u>		FTS		GFCS	MET		COMMENTS
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Path	length n)	i	La sera	# Lines Measured	Time	Spectral Interval	Code*	GFCS	ppH ₂ 0 (Torr)	visibility (km)	
1000-1505 " 123 x 14.5 25.0 1100-1545 HeNe, YAC, prof. pr	35	080	0950-1715	HeNe,YAG, CO, CO ₂	544	1	1	1	×	15.0	26.0	·
1100-1545 94Ne,YAG, 26 1120 1800-6600 311 X 14.0 28.0 1.00-1545 9.5 1.00-1540		<u>.</u>	1000-1500	=	123	;	;	;	×	14.5	25.0	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			1100-1545	Hene, YAG, DF	56	1120	1800-6600	31.1	×	14.0	28.0	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	•	•	1	:	1	1350	1800-6600	311	×	14.5	:	
0930-1410 HeNe, YAG 42 1015 1800-3202 311 X 16.5 18.0 1245 1800-3200 311 X " " 1300 1800-3200 311 X " " 1420 1800-3200 311 X " " 1420 1800-3200 311 X 18.0 " 1115 2000-2050 911 X 18.0 % 1215 2000-2050 911 X 18.0 " 1215 2000-2050 911 X 18.0 " 1210 1800-3200 311 X 18.0 " 1645 1800-3200 311 X 19.0 " 1145<	•		;	;	;	1415	1800-6600	311	×	14.5	:	
1245 1800-3200 311			0930-1410	HeNe, YAG DF	7,7	1015	1800-3203	311	×	16.5	18.0	
1300 1800-3200 311			;	:	;	1245	1800-3200	311	×	÷	ż	
1420 1800-1200 111	-		;	;	;	1300	1800-3200	311	×	:	=	
0900-1615 HeNe, YAG 84 0910 1800-6600 311 X 18.0 46.0 1115 2000-2050 911 X 18.0 " 1215 2000-2050 911 X 18.0 " 1310 800-3200 311 X 17.0 " 1330 1800-6600 311 X 17.0 " 1645 1800-6600 311 X 18.0 " 1645 1800-5600 311 X 18.0 " 1145 1800-3200 311 X " " 1210 1800-3200 311 X " "	-		i	:	;	1420	1800-3200	311	×	:	±	
			0900-1615	HeNe,YAG DF,CO,CO ₂	78	0810	1800-6600	311	×	18.0	0.97	
1215 2000-2050 911 X 18.0 1310 800-3200 311 X 17.0 1330 1800-6600 311 X 17.0 1645 1800-6600 311 X 18.0 0845-1515 HeNe, YAC 80 0900 1800-3200 311 X 20.0 1145 1800-3200 311 X 20.0 1145 1800-3200 311 X "" 1145 1800-3200 311 X ""	_	<u>.</u>	:	;	;	1115	2000-2050	911	*	18.0		O laser scans on FTS
1310 800-3200 311 X 17.0 1330 1800-6600 311 X 17.0 1645 1800-6600 311 X 18.0 0845-1515 HeNe, Y4C 80 0900 1800-3200 311 X 20.0 1145 1800-3200 311 X 20.0 1210 1800-3200 311 X " 1145 1800-3200 311 X "		<u>.</u>	:	;	ł	1215	2000-2050	911	×	18.0	=	
1330 1800-6600 311 X 17.0 0845-1515 HeNe,YAC 80 0900 1800-5200 311 X 20.0 1145 1800-3200 311 X 20.0 1145 1800-3200 311 X "" 1210 1800-3200 311 X "" 1210 1800-3200 311 X ""			1	;	!	1310	800-3200	311	×	17.0	=	
1645 1800-6600 311 X 18.0 0845-1515 HeNe.Y4C 80 0900 1800-3200 311 X 20.0 1145 1800-3200 311 X " 1210 1800-3200 311 X " 1210 1800-3200 311 X "		:			;	1330	1800-6600	311	×	17.0	=	
0845-1515 HeNe,Y4G 80 0900 1800-3200 311 X 20.0 1145 1800-3200 311 X " 1210 1800-3200 311 X " 1535 1800-3200 311 X "		:	;	;	;	1645	1800-6600	311	×	18.0	:	
1145 1800-3200 311 X " " 1210 1800-3200 311 X " 1535 1800-3200 311 X " " 1535 1800-3200 311 X "		:	0845-1515	HeNe,Y4G DF, CO ₂	90	0060	1800-3200	311	×	20.0	32.0	
1210 1800-3200 311 X " 1535 1800-3200 311 X "		:	}	1	ł	1145	1800-3200	31.1	×	:	=	
1535 1800-3200 311 X "			:	;	1	1210	1800-3200	311	×	=	=	
		=	1	1	r •	1535	1800-3200	31.1	×	=	Ξ	

TABLE 1.1. 1977 CCAFS EXPERIMENT SUPMARY

STRAKHOO					multi-line DF laser on FTS		
	ppH ₂ O visibility (km)	27.0	=	:	£ !	ł	1
MET	ppH ₂ 0 (Torr)	20.0	:	20.0	;	ł	;
GFCS	GFCS	×	×	×	1	Ļ	:
	Code*	311	311	311	911	311	311
FTS	FTS Spectral Interval (cm ⁻¹)	0955 1800-6600	1800-6600	1800-6600	1800-3200	1800-6600	1445 1800-3200
	Time	0955	1155	1215	1050	1430	1445
ER	# Lines Measured	51	;	:	109	1	:
LASER	Lasers	0845-1345 HeNe,YAG DF, CO ₂	ŀ	;	HeNe,YAG DF,CO ₂	1	;
	Time	1845-1345	1	1	0950-1500	;	!
	Date Pathlength (m)	\$080	=	=	20 0	2	=
	Date	\$-2\$			56		

NOTES:

+ several interferrograms recorded and stored but not yet transformed

FTS measurement code

1st digit: source

0 = no source
1 = transmitter greybody
2 = receiver greybody
3 = globar (transmitter)
9 = as specified in comments

2nd digit: beamsplitter

1 = CaF₂ 2 = Quartz 3 = KBr

.rd digit: detector

1 = InSb (SBRC) 2 = HgCdTe (ADL) 3 = HgCJFe (TI)

TABLE	2.8 OF	LINE BY L	INE LASER	EXTINCTIO	N MEASUREM	ENTS FOR HE	NE LASER	SOURCE
DATE	T II1E	RUN CODE	LASER	LINE ID	MOB GAIN	STAT GAIN	TRANS	EX COEF
32M77	953	7	a	P00-51	0	0	0.747	0.857
921177	954	3	0	P00-SI	0 0 0	0	0.757	0.054
921177	1111	3	0	P90-S1	Ø	e	0.718	0.065
32M77 88M77	1216 9 3 7	3 7	ម	P00-51 P00-51	9	9	0.646	0.085
23177	939	3	ดั	P00-51	i	ä	0.534 0.529	0.123 0.124
n81177	941	3	ĕ	P00-51	î	ĕ	0.526	0.126
78477	943	3	Ø	P00-S1	i	Ø	ด.539	0.121
n6i177	945	3	Ø	P00-S1 P00-S1	1	ø	0.521	0.127
38M77 08M77	947 1356	3	Ø	P00-51	1	9	0.533	0.123
38M77	1358	4	Ö	P00-51 P00-81	D D	e e	0.597 0.579	0.101 0.107
84M77	1446	3	ă	P00-51	ă	ä	0.456	0.153
19M77	1155	3	ē	P00-SI	ž	ž	0.154	0.365
11M77	1356	3	Ð	P00-SI	2	2	0.314	0.365 3.226
11'177	1449	3	9	P00-31	2	2	0.282	0.247
12M77 12M77	1402 1505	3	9	P00-SI P00-SI	2	2	0.429	0.165
15M27	837	3	ä	P00-SI	5	5	0.430	0.165 0.132
31:177	1511	3	ĕ	12-004	2	ž	0.562	0.113
91977	1438	4	ē	P00-51 P00-51	ã	ž	0.509 0.562 0.383	0.188
62A77	1151	3	Ø	P00-SI	2	2	0.516 0.519	0.129
92A77 92A77	1235	4	õ	P00-51	Š	2	0.513	0.128
02H77	1314 1420	5	ับ ด	P00-SI F00-SI	<u></u>	5	0.546 0.565	0.118 0.111
92A77	1582	ĕ	ĕ	P00-S1	2 ع	2 -	0.581	0.106
0-iH77	1052	3	ě	P00-51	ž	ž	0.581 0.512	0.131
04877	1133	4	ø	P00-S1	ž	Š	0.548	0.117
04477 04 4 77	1451 1538	5	9	P00-SI	2	2	0.407	0.175
94A77	1617	4	ย	P00-SI P00-SI	5	5	0.384 0.341	0.187 0.210
95a77	1.450	3	ĕ	Puú-ST	2	2	0.678	0.076
95H77	1527	4	ē	₽50 -ST P00-SI	Ž	ž	0.678 0.730	0.061
13Y77	1243	3	ō	P90-SI	ب	2	0.673	0.076
16Y77	1444 1530	4	9	P00-SI P00-SI	ļ	1	0.557	0.114
1€ Y77 17Y77	1233	2	Ø	P00-51	1	1	0.559 0.497	0.114 0.137
29577	1438	3	ĕ	P00-51	ž	2	0.582	0.107
21Y77 21Y77	1130	ž	ø	P00-S1	ž	ž	R. 42R	0.166
21777	1207 1329	4	Ø	P00-S1	ã	2	0.436	0.162
21477	1329	5	Ø	P00-S1	5	5	0.420	0.169
21Y77 23Y77	1359 1236	6	Ø	P00-51 P00-51	Š	2	0.409 0.840	0.175 0.334
23Y77	1435	<u> </u>	ลั	P00-51	5	5	0.728	0.062
23777	1602	ĕ	ě	P09-S1	ž	ž	0.790	0.046
24477	1435 1602 1 03 9	3	0	P00-S1	2	2	0.716	0.065
24Y77 24Y77	1119	ĸ.ºINNMMMMMA 4 MMMMMMMMMMA A TO GOM 4 ID G GM 4 ID G	හිත ම ම ම ම ම ම ම ම ම ම ම ම ම ම ම ම ම ම ම	P00-51	NNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNN	ชอยออออออออออออออออออดดดดดดดดดดดดดดดออออออ	0.730	0.062
24Y77 24Y77	1328 1409	ž	ช ด	P00-SI P00-S I	5	2	0.661 0.730	0.081 0.062
24Y77	1503	ě	ă	P00-51	5	ź	0.730 0.720	0.064
25Y77	847	ž	ě	P00-S1	ž	ž	0.526	0.125
25Y77	930 1006	4	ø	P00-51	2	2	0.642	0.086
25Y77	1006	5	0	P00-S1	Š	2	0.654	0.083
25Y77	1143	6	0	P00-5 I	2	2	0.615	ø.095

TABLE	3.1 CF	TINE BA T	ine theek	EXTINCTIO	n measurem	ents for ND	VG LASER	Source
DATE	TIME	BUN CODE	Laser	FINE ID	MOB GAIN	STAT GAIN	Trans	en coef
02077	1154	\$160 G	ŧ	P11-51	ž	だまでまかまでしたとの むいたいできたい てょうきのまのものものものものも	0.683	0.075
02017	1528	5	1	F11-\$1	אַ פַּפָּט בין אַפָּט שַּיי פַֿיי פֿין פּפּ פּט פּט פּט פּט פּט פּט פּט פּט פּ	2	0.665	0.001
DEATY	1315	Ģ	3	611=21	Ę	Š	0.677	0.076
17650	1455		•	Pii-Si	₹	₹	0.671	0.078
Tracq	1505	Ď	į	F11-51	Š.	Š	0.639	0.097
OZATT	1517	b S	1	F11-1H	3	79	9.631	669.0 886.0
02477	1545	e e	1	P11-IN P11-S1	3	¥1	0.637 0.5 84	0.185
0-16-17	1054 1134	3	1	F11-31	<u> </u>	<u>t</u> .	0.577	9.107
O-AATT	1453	066516	ŧ	F11-51	Š	ž	0.440	9, 160
04477	539	ă	i	FII-SI	5	Š	0.418	0.171
0.4077	1618	4	i	řii-ši	3	3	0.369	ð. 195
คริกก	1450	3	i	Pii-ši	į	Š	Ŭ.PAP	0.057
05A77	isää	ä	ì	Pii~ši	ž	2	0.799	0.044
05977	157g 157	5	Ì	Pii-in	Ž	Ž	0.830	0.036
161777	15.16	ない さい 二 だいさい そいきいきゅう 丁	ĺ	111-51	2	ē	0.896	156.0
16/11	1446	ન	1	F11-51	1	١	0.793	0.045
16/27	1533	5	l	Pliast	3	l l	0.773	0.050
14/130	1535	3	1	P11-91	Š		0.658	589.0
30177	1440	3	ļ	F11-51	₹	Ĩ.	8,764	0.053
30/17	1530	3	1	P11-51	Ę	ę	0.790	0.049
21/ma 21/ma	1133	3	1	P11-51	હુ	() (() + () + () + () + () + () + () +	0.710	0.067
\$1725	1300	년	1	F11-5!	Ę.	ž	0.696 n.693	0.071 0.072
341,000	1331	5	į.	P11=\$1 P11=\$1	ž	5	0.641	0.005
3:175	1139	b Z	;	P11-\$1		5	0.781	949,9
	1232	3	;	F11-51	<u> </u>	Š	0.759	0.054
3900	1423	45	i	Pil-Si	3	Ë	0,723	9.063
3.4.10	1604	9	i	Pii≥ŝì	3	3	ő, TSÍ	0.061
3417	1036	Š	i	řii~ši	,	ê	4.755	0.055
3411	กำเรี	4	į	Fil-Si	ğ	3	0,745	0.057
2.1/11	1331	4 6	ĺ	P11-51	Walinda Cura Cura Cura Mana Gara Cura Mana Cura Cura Mana Cura Cura Cura Cura Cura Cura Cura Cur	ر) ودود: الارد	0.734	0.060
39/100	1412	ij	Í	ri1-51	3	5	0.743	929.0
34/23	1594	6	1	Pil-St	4	30000	0.716	0.065
28177	848	3	1	F11-51	احاتا م اعاد	2	0.615	0.095
3617	33.	ન	1	P11-41	Ş	7	0.731	0.061
3代人標準	1010	€,		P11×41		3	0.731	0.861

TABLE	5.5 OF	LINE BY L	INE LASER	EXTINCTIO	N MEASUREM	ents for df	LASER	SOURCE
PATE	TIME	FUN CODE	Laser	LINE ID	MOB GAIN	STAT GAIN	TRANS	EX COEF
23000000000000000000000000000000000000	29 143356799814444444 144356798914444444 144457455689 14435675689 155059 155059	o rambiol i madamotecalamendo el almestada esta	иолимоминатарманамамамаманамамамамамамамамамамамама	P07-987-987-987-987-987-987-987-987-987-98	44 <i>55555554</i> 465566666666544644	3044444748885444445444888588	8.4348827552916599748898446677529165997488984444891534566666666666666666666666666666666666	0.144 0.1482 0.1491 0.1491 0.1502 0.1503 0.1503 0.1504 0.1504 0.1504 0.1504 0.1504 0.1504 0.1504 0.1504 0.1504 0.1504 0.1504 0.1504 0.1504 0.1504 0.1505 0.1504 0.1506 0.1
\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	2446804135679068444458790444444444444444444444444444444444444	19966999669999999999999999999999999999	ษองผพพพพพพพพพพพพพพพพพพพพพพพพพพพพพพพพพพพพ	P022-08 P021-067 P001-067 P001-067 P001-067 P001-067 P002-06 P002-068 P002-068 P002-068 P002-068 P002-068 P002-068 P002-08 P00	M44546666544448MAMAMA55544M447C	88844555544887688888474474886466	0.446336668779961996459475240737964595454454596459379666966654596452155207379655334	9.091 9.145 9.1095 9.1095 9.1092 9.1094 9.1094 9.1094 9.1094 9.1094 9.1094 9.1094 9.1094 9.1094 9.1097 9.10

Table	2.2 OF	LINE BY L	INE LASER	EXTINCTION	ON MEASUREM	ents for Df	Laser	SOURCE
DATE	TIME	RUN CODE	LASER	LINE ID	MOB GRIN	STAT GAIN	TRANS	EX COEF
09H777 09M77 09M77 09H77 09H77 09M77 09M77 09M77 09M77 09M77 09M77 09M77	16221 16221 16221 16221 16226 16226 16226 16226 16226 16237 16337	លសមាលមាលមាលមាលមាល	ыстывавававиты В предериения	P02-05 P01-05 P01-05 P01-06 P01-07 P01-09 P01-09 P02-07 P02-10 P02-10 P02-10 P02-10	<i></i> 5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5	4466666666664464646	0.540 0.385 0.585 0.537 0.5486 0.537 0.5418 0.5418 0.5439 0.5439 0.5439	0.118 6.187 0.121 0.201 0.105 0.144 0.105 0.194 0.107 0.162 0.158 0.117 0.161
11M77	1129 1123 1133 1134 1145 1155 1155 1155 1155 115	мпромомомомом 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	амимамамамамамамамамамамам	P053-1-1-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-	4447677@4446444448785564	ผนผนาดอน เผนผนนผนผน เล่น ด เราแนน	0.358 0.358 0.357	8.201 9.161 9.184 9.188 9.2146 9.2146 9.235 9.262 9.162 9.136 9.136 9.136 9.136 9.136 9.148 9.156
12M27 12M27 12M27 12M27 12M27 12M27 12M27 12M27 12M27 12M27 12M27	158245098 158225098 15822861355 1582	പരേരമയത്തെയ്ത്തെയ്യ	លក្ខសាធានាធានាធានាធានាធានាធានាធានាធានាធានាធា	P02-08 P02-07 P02-05 P01-08 P01-06 P01-07 P01-08 P02-05 P02-98 P02-10 P02-10 P02-10	4440606055564448	48000000000000000000000000000000000000	0.525 0.497 0.497 0.249 0.559 0.541 0.548 0.519 0.328 0.598 0.593 0.401 0.506	0.126 2.219 0.137 0.272 0.123 0.129 0.125 0.227 0.128 0.128 0.128 0.128 0.128 0.134 0.179 0.133

TABLE	2.2 OF	LINE BY L	INE LASER	EXTINCTION	ON MEASUREM	ENTS FOR DF	LASER	SOURCE
PATE	TIME	RUN CODE	Lasex	LINE ID	MOB GAIN	STAT GAIN	TRANS	EX COEF
14/77 14/77 14/77 14/77 14/77 14/77 14/77 14/77 14/77 14/77 14/77 14/77	1110 11112 11114 11116 11116 11116 11123 1123 1123 1123	ଜନ୍ୟଗମସର ପ୍ରବଳକ ଜନ୍ମର ବ	<u>अवज्ञानम्बर्धानम्बर्धानम्बर्ध</u>	P02-08 P02-07 P02-05 P01-08 P01-07 P01-06 P01-07 P02-07 P02-07 P02-08 P02-10 F02-10 F02-08	8876666855494667	™™451266660004000044	0.693 0.594 0.662 0.541 0.666 0.661 0.527 0.674 0.507 0.507 0.507	0 072 0.102 0.030 0.120 0.079 0.081 0.125 0.077 0.111 0.066 0.133 0.087 0.153
15M77 15M77 15M77 15M77 15M77 15M77 15M77 15M77 15M77 15M77 15M77 15M77	181 ! 1013 1014 1015 1016 1017 1018 1019 1321 1025 1025 1026 1029	ଜଣନାଧାନାନାନାନ୍ୟକ୍ରକ୍ଷାନାନାକାର	asaaasaaaaaaaaa	P02-08 F02-57 P02-35 P01-09 P01-07 P01-07 P01-38 P02-35 P02-37 P02-10 P02-10 P02-10 P02-10	ринк өссө тартыры	the colored to the telephone of telephone of the telephone of the telephone of tel	0.718 0.536 0.679 0.475 0.582 0.475 0.475 0.563 0.516 0.517 0.647	8.067 6.122 6.676 6.146 6.873 6.146 6.080 6.146 6.080 6.129 6.091 6.129 6.085
THE STATE OF THE S	1484 1412 1414 1415 1416 1416 1419 1423 1423 1424 1425 1426 1427	ଊ୶ଊ୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷	अवकाषां वाचा वाचा वाचा वाचा वाचा वाचा वाचा	P02-08 P02-07 P02-05 P01-08 P01-07 P01-06 P01-08 P02-05 P02-07 P02-08 P02-10 P02-10 P02-10	\$551-671-855544644	MM40000004MMMMMM	0.634 0.399 0.640 0.286 0.622 0.487 0.617 0.288 0.635 0.635 0.485 0.485 0.492 0.644	0.089 0.180 0.087 0.245 0.093 0.194 0.243 0.188 0.188 0.141 0.098 0.153

DATE	TIME	RUN CODE	E LASE	R LINE I	TION MEASURI	MENTS F	OR DF	LASER SOURCE
01477	1312			··· Line [NI AD BOM G	STAT	GAIN T	RANS E. COEF
01477 01477	1214 1214 1218 12218 1222 1222 1222 1222	мюммммммммммачьтата тататата	имимимене веременте	P02-05 P01-08 P01-08 P01-08 P01-08 P02-10 P02-12 P02-12 P02-05 P01-07 P01-07 P01-07 P01-08 P02-08 P01-08 P01-08 P01-08 P01-08 P02-12 P01-08 P02-12 P02-08	6	~~05068444466688460666644846868	80000000000000000000000000000000000000	.672
02677 12		WO WEDDINGS.	ON TOWNS TOWN TOWNS TO THE TOWN TOWNS TO THE TOWN TOWNS TOWN	92-10 33-00	444%\@\\&5555\\\5545659&&&&\$5655\\44) MMM661666444664M444111111111111111	0.45444900000000000000000000000000000000	6 0.060 6 0.153 0 0.856 0 0.268

TABLE	S.2 OF	LINE BY L	INE LASER	EXTINCTION	N MEASUREM	ents for DF	LASER	SOURCE
DATE	TIME	RUN CODE	Laser	LINE ID	MOB GAIN	STAT GAIN	TRANS	EX COEF
04A???	1151 1153 1155 1155 1156 1157 1158 1159 1202 1206 1207 1404 1410 1411 1418 1419 1423 1425 1427 1429 1430	ВВВВВВВВВВВВВВВВВВВВВВВВВВВВВВВВВВВВ	୶ଊୠୠୠୠୠୠୠୠ୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷	P02208 P02208 P02208 P001112 P001112 P001208 P002209 P001119 P001119 P001119 P001119 P001119 P001119 P001119 P001119 P001119 P001119 P001119 P001119 P001119 P001119 P001119 P001119 P001119	4447664684734556588698956558955	のいのりりりのちゃんのくかするいとととのでとすすするとすず	2246847966178666424698873110801774 676874966178666424698873110801774 900000000000000000000000000000000000	0.099 0.193 0.243 0.1087 0.1573 0.1153 0.1158 0.1158 0.1264 0.1269 0.1264 0.1269 0.1279 0.1279 0.1356 0.1356 0.1356 0.1356 0.1359 0.1359 0.1359
05A77 05A77 95A77 95A77 95A77 95A77 95A77 95A77 05A77	1540 1541 1543 1544 1545 1546 1548 1549 1550 1551	мамамамам	мамамамама	P02-08 P02-07 P02-05 P01-08 P01-06 P02-08 P02-10 P02-12 P02-38	5577775575	4466664464	0.834 0.613 0.819 0.784 0.784 0.685 0.617 0.617 0.7814	0.036 0.096 0.039 0.118 0.047 0.074 0.036 0.094 0.054
20Y77 20Y77 20Y77 20Y77 20Y77 20Y77 20Y77 20Y77 20Y77 20Y77	1502 1504 1506 1508 1509 1512 1514 1516 1518	применения	мманананам	P02-08 P02-07 P02-05 P01-08 P01-07 P01-06 F02-08 P02-10 P02-12 P02-08	3357693483	NOIMNONDEN	0.558 0.588 0.540 0.296 0.539 0.441 0.549 0.425 0.558	0.114 0.185 0.120 0.238 0.121 0.160 0.117 0.167 0.114 0.118

	LINE LASER E	XTINCTION MEA	SUREMENTS FOR	R DF GAIN T	Laser sour	
DATE TIME RUN COD 21Y77 1146 3 21Y77 1147 3 21Y77 1149 3 21Y77 1151 3 21Y77 1153 3 21Y77 1158 3 21Y77 1159 3 21Y77 1200 3 21Y77 1201 3 21Y77 1203 4 21Y77 1341 4 21Y77 1342 4 21Y77 1343 4 21Y77 1344 4 21Y77 1343 4 21Y77 1344 4 21Y77 1350 4 21Y77 1350 4 21Y77 1350 4 21Y77 1350 4					2.260 2.260 3.325 3.342 8.689 8.689 8.691 8.695 8.695 8.670 8.670 8.684 8.665 8.665 8.684 8.665 8.684 8.685 8.684 8.685 8.6865 8.6865 8.6866 8.	.188 .263 .186 .1299 .073 .073 .072 0.149 0.074 0.074 0.080 0.161 0.082 0.161 0.082 0.161 0.082 0.161 0.082 0.161
21Y77 1354 4 23Y77 1221 3 23Y77 1222 3 23Y77 1222 3 23Y77 1225 3 23Y77 1226 3 23Y77 1227 23 23Y77 1229 3 23Y77 1229 3 23Y77 1230 3 23Y77 1231 23 23Y77 1243 23Y77 1445 23Y77 1446 23Y77 1445 23Y77 1451 23Y77 1451 23Y77 1452 23'77 1452 23'77 1457 23Y77 1457		P02-08 P02-07 P02-05 P01-08 P01-07 P02-08 P02-10 P02-12 P02-08 P02-08 P02-07 P02-05 P01-08 P01-08 P01-06 P01-06 P02-10 P02-12 P02-12	47476744644157674464	™™™®®™™™™™™™™™™™™™™™™™™™™™™™™™™™™™™™™	0.673 0.439 0.679 0.656 0.494 0.687 0.637 0.631 0.657 0.6517 0.6517 0.6613 0.645 0.645	0.077 0.161 0.076 0.218 0.084 0.133 0.099 0.135 0.099 0.079 0.082 0.171 0.079 0.224 0.075 0.130 0.089 0.137 0.086 0.092
24Y77 1047 24Y77 1052 24Y77 1053 24Y77 1054 24Y77 1057 24Y77 1059 24Y77 1093 24Y77 1102 24Y77 1103 24Y77 1104 24Y77 1341 24Y77 1342 24Y77 1345 24Y77 1346 24Y77 1346 24Y77 1350 24Y77 1350 24Y77 1350 24Y77 1354 24Y77 1355	© B B B B B B B B B B B B B B B B B B B	P02-08 P02-07 P02-05 P01-08 P01-07 P01-06 P02-10 P02-12 P02-10 P02-08 P02-08 P02-07 P01-08 P01-07 P01-08 P01-07 P01-08 P01-07 P01-08 P01-08 P02-08	445009946045551995895	00418785994478884	9.557 9.333 9.559 9.495 9.495 9.559 9.559 9.5533 9.5536 9.5538 9.538	0.100

TABLE	2.2 OF	LINE BY L	INE LASER	EXTINCTION	ON MEASUREM	ENTS FOR DF	LASER	SOURCE
DATE	TIME	RUN CODE	LASER	LINE ID	MOB GAIN	STAT GAIN	TRANS	EX COEF
25Y77 25Y77 25Y77 25Y77 25Y77 25Y77 25Y77 25Y77	1036 1035 1036 1133 1134 1136 1139 1140	пвининия.	***************************************	P02-08 P02-07 P02-05 P01-06 P02-12 P02-10 P02-08	55655755	4 4 4 4 5 4	0.590 0.370 0.339).448 0.589 0.468 0.587	0.103 0.194 0.211 0.157 0.104 0.103 0.148 0.104
TABLE	2.3 OF				on Measurem			SOURCE
DATE	TIME	RUN CODE	LASER	LINE ID	MOB GAIN	STAT GAIN	TRANS	EX COEF
16Y77 16Y77 16Y77 16Y77	162 0 1631 1636 1640	3533	4 4 4 4	P05-09 P04-10 P04-09 P04-08	2 12 2 2	8 9 9	0.035 0.046 0.191 0 106	0.654 0.601 0.323 0.319
17 Y77 17 Y77 17 Y77 17 Y77 17 Y77 17 Y77	1247 1250 1254 1259 1301 1302 1303	3383888	4 4 4 4 4	P04-09 P04-11 P05-11 P04-10 P04-09 P04-08	8888888	SUNNAND	8.004 0.007 0.004 0.010 0.010 0.047 0.048	1.091 0.957 1.078 0.899 0.899 0.597 0.593
23Y77 23Y77 23Y77 23Y77	1148 1150 1156 1200	3 3 3 3	4 4 4	P04-09 P04-08 P04-10 P05-09	12 12 12 12	9 9 9	0.113 0.121 0.021 0.015	8.425 8.413 8.759 8.818

TABLE	2.4 OF	LINE BY L	INE LASER	EXTINCTIO	ON MEASUREM	ENTS FOR CO2	Laser	SOURCE
DATE	TIME	RUN CODE	Laser	LINE ID	MOB GAIN	STAT GAIN	TRANS	EX COEF
02M77 02M77	1118 1120 1121 1123 1125 1127 1128 1130 1134 1139 1143 1143 1144 1157 1146 1157 1158 1203 1207	мамамамамамамамамаман м	<i></i> ອກຈອກອກຈອກຈອກອກສອກສອກ	P10-26 P10-30 P10-38 P10-19 P10-106 R10-34 R10-28 R10-12 R10-22 R12-26 P022-32 P022-14 P022-14 P022-14 P022-14 P022-14 P022-14 R022-08	**************************************	RNURNENTERFERENCERRE	8.567 8.6613 8.6644 8.785 9.535 8.6619 9.857 8.630 9.394 9.537 9.537 9.537 9.537 9.537 9.537 9.537 9.537 9.537 9.537 9.537 9.536 9.537 9.5	0.111 0.096 0.068 0.122 0.106 9.081 0.094 0.5587 0.167 0.181 0.159 0.181 0.120 0.121 0.202 0.129 0.121
08M77708M77708M77708M77708M77708M77708M77708M77708M77708M77708M77708M77708M77708M77708M77708M77708M777	1019 1010 1022 1024 1025 1028 1033 1033 1033 1034 1034 1044 1044 1044	им	<i>ចង្គមានមានមានមានមានមានមានមាន</i>	P10-20 P10-30 P10-38 P10-14 P10-10-66 R10-20 R10-28 R10-20 R10-28 R10-28 R10-28 R10-28 R10-32 R10-32 R10-32 R10-32	~~~8666688666744554355	656655554545BBBBBBRANNB	0.389 0.417 0.437 0.251 0.374 0.395 0.4480 0.113 0.4441 0.24340 0.2484 0.2484 0.350 0.397 0.406 0.397 0.406	0.184 0.171 0.162 0.270 0.192 0.182 0.182 0.184 0.426 0.159 0.211 0.177 0.246 0.205 0.180 0.428
09M??	1512 1513 1515 1517 1519 1520 1521 1522 1524 1526 1537 1538 1541 1553 1554 1554 1556	момомомомомомомомомом	ម្នានមានមានមានមានមានមានមានមានមានមានមានមានម	P10-29 P10-36 P10-38 P10-14 P10-10 P10-06 R10-34 R10-28 R10-28 R10-06 P02-32 R10-28 R10-46 P02-36 P02-32 P02-32 P02-34 P02-28 R02-28 R02-28 R02-28	777988878576555555575	5557666644456888888888888888888888888888	0.313 0.343 0.357 0.364 0.315 0.325 0.413 0.975 0.644 0.265 0.287 0.244 0.233 0.274 0.335 0.035 0.339	0.227 0.209 0.201 0.197 0.219 0.219 0.173 1.091 0.322 0.059 0.254 0.211 0.318 0.273 0.214 0.214 0.253

TABLE	2.4 OF	LINE BY L	INE LASER	EXTINCTIO	N MEASUREM	ENTS FOR CO2	LASER	SOURCE
DATE	TIME	RUN CODE	Laser	LINE ID	MOB GAIN	STAT GAIN	TRANS	EX COEF
10M77	1349 1354 13554 13559 1480 14403 14413 14414 1436 1436 1445 1450 1450 1456	анаыныныныныныныныны	មានមានមានមានមានមានមានមានមានមានមានមានមានម	P18-28 P18-38 P18-38 P18-26 P18-28 P18-14 P18-06 R18-28 R18-28 R18-22 P18-26 P18-26 P18-26 P18-26 P18-26 P18-26 P18-26 P18-26 P18-26 P18-26	900019999000177776669669	@~~~@@@~@@# <i>5</i> #5#4######	8.188 0.214 0.203 0.076 0.169 0.206 0.105 0.236 0.236 0.236 0.231 0.178 0.162 0.178 0.183	9.301 9.301 9.311 9.503 9.325
11M77 11M77 11M77 11M77 11M77 11M77 11M77 11M77 11M77 11M77 11M77 11M77 11M77 11M77 11M77	1486 1412 1415 1416 1418 1419 1426 1427 1428 1431 1433 1434 1444 1444 1445	имамамамамамамамамамамамамамамамамамама	<i></i>	F10-20 F10-26 F10-30 F10-38 F10-38 F10-38 F10-38 F10-10 F10-28 R10-28 R10-28 R10-23 P02-20 F02-32 F02-32 F02-14 F02-08 R02-20 R02-20	188899888687655664484	######################################	0.142 0.147 0.158 0.167 0.161 0.176 0.375 0.189 0.208 0.207 0.207 0.250 0.250 0.239	0.381 0.3860 0.3560 0.3559 0.3559 0.3339 0.5335 0.3355 0.3356 0.3366 0.3667 0.3667 0.3667
12M77	1428 1429 1431 1432 1433 1434 1436 1443 1446 1449 1451 1453 1454 1455 1455 1458	пинаминаминаминами	សមាលមានសមានសមានសមានសមាន	P18-20 P10-30 P10-30 P10-34 P10-06 R10-34 R10-28 R10-16 P02-20 P02-32 P02-14 P02-28 R02-28 R02-28	@&&&@@@&\$\55555555	55555554444BBBBBBBBBB	0.482 0.514 0.524 0.524 0.574 0.5725 0.681 0.590 0.649 0.649 0.727 0.698 0.727	0.142 0.130 0.119 0.126 0.146 0.149 0.063 0.075 0.293 0.085 0.085 0.062 0.070 0.034 0.044 0.044

TABLE	2.4 OF	LINE BY L	INE LASER	EXTINCTIO	N MEASUREN	ENTS FOR CO2	LASER	SOURCE
DATE	TIME	RUN CODE	Laser	LINE !D	MOB GAIN	STAT GAIN	TEANS	EX COEF
**************************************	1150 1151 1152 1153 1155 1156 1157 1158 1200 1201 1203 1204 1208 1209 1211 1208 1209 1211 1213 1448 1449 1451 1458 1503 1503 1503 1503 1503 1503 1503 1503	проводиний в в в в в в в в в в в в в в в в в в в	<i></i>	066884406488426624480884366044066220884426664888496624888442666226842664888408262488842666288426662888426662888488884888848888488888888	©©©©©©©©©™©©©©®¶®®™©©©©™©©©©©©©©©©©©©©©	$oldsymbol{ int}$	9.54339762335423503521044854767381135667298505394134666 0000000000000000000000000000000000	0.136 0.119 0.199 0.199 0.153 0.127 0.123 0.1242 0.2247 0.2247 0.2247 0.2247 0.157
15M77715M77715M77715M77715M77715M77715M777715M777715M777715M777715M7777715M7777715M77777777	907 908 909 910 9112 914 914 917 919 922 928 933 933 933	иамисимимимимимими	ភភភភភភភភភភភភភភភភភភភភភភភភភភភភភភភភភភភភ	P10-20 P10-33 P10-33 P10-14 P10-10-06 R10-20 R10-22 R10-22 R10-20 R10-23 R10-28 R02-26 P02-28 R02-28 R02-28 R02-38	87776666256555555564	©©©©©©©™™™™™™™™™™™™™™™™™™™™™™™™™™™™™™™	0.3735 0.4459 0.4459 0.4459 0.3544 0.4469 0.42247 0.42	8.193 0.177 0.158 0.214 0.152 0.164 0.166 0.251 0.259 0.259 0.256 0.259 0.256 0.259

TABLE	2.4 OF	TIME BA T	INE LASER	EXTINCTIO	n measurem	ents for co2	Laser	SOURCE
DATE	TIME	RUN CODE	LASER	LINE ID	MOB GAIN	STAT GAIN	TRANS	EX COEF
01A77 01A77 01A77 01A77 01A77 01A77 01A77 01A77 01A77 01A77 01A77 01A77	1449 1450 1451 1452 1453 1455 1455 1459 1500 1500 1500 1500 1500 1500 1500 15	494914	២២២២២២២២២២២២២២២២២២២២២២២២២២២២២២២២២២២២២២២	P18-28 P18-28 P18-38 P18-18 P18-18 P18-34 R18-28 R18-28 R18-28 P02-28 P02-28 P02-28 P02-28 P02-28 P02-28 P02-28 P02-28 P02-28 R02-28 R02-8 R02-8	102999888797766666660 106	@\$@\$##################################	0.121 0.136 0.138 0.146 0.121 0.160 0.194 0.175 0.154 0.160 0.179 0.179 0.219 0.219	24997 44997 43987 63387 44388 60388 6038 6038 6038 6038 6038 6038
77777777777777777777777777777777777777	12499 12499 125523345 1255550 1255550 1255550 1255550 1255550 1255550 1255550 1255550 1255550 1255550 1255550 1255550 1255550 1255550 1255550 1255550 1255550 1255550 125550 125550 125550 1255550 125	мюмммммммммммммммммчччччччччччччч	សសមាមមានមានមានមានមានមានមានមានមានមានមានមានម	20 - 260 - 2	കയെയെയയയെന്റ് മത്താന് പ്രപാരം നേതനാന് മയയയെയെയെയെയെയെയെയെയെയെയെയെയെയെയെയെയെയെ	######################################	8.1294487 1294487 1294487 1294	\$66052462484598155229511009931.1.* 21-1800666 \ 951864884598155229511009931.1.* 21-1800666 \ 9518648845366498155229511009931.1.* 24-1800666 \ 95186488455566496667 \ 95186486697 \ 4866

Taple	2.4 OF	LINE BY L	INE LASER	EXTINCTIO	N MEASUREM	ents for cos	LASER	SOURCE
DATE	TIME	RUN CODE	LASER	LINE ID	MOB GAIN	STAT GAIN	TRANS	EX COEF
**************************************	7.8990011333890023456790126689244679128047912558025802 111111111111111111111111111111111111		រ អ្ន សភាគមានការប្រភពភាគមានការបានការបានការបានការបានការបានការបានការបានការបានការបានការបានការបានការបានការបានការបានការបា ក្រុម	P110-192824088408840884088408840884088408840884	หน้า เราะ เราะ เราะ เราะ เราะ เราะ เราะ เรา	# # # # # # # # # # # # # # # # # # #	8.14624285188188118412264703552548188188414378836412226670355254818818818841437883641222667035525481818181818181818181818181818181818181	77585557414442235762357623577578883599353757414444473357693776933774144447732676937769377793677783883599377785778777877787778777957795777957
04477	1615	4	5	F10-20	8	5	0.110	0.431
05A77 05A77 05A77 05A77 05A77 05A77 05A77 05A77 05A77 05A77 05A77 05A77 05A77 05A77 05A77	1502 1503 1504 1506 1507 1508 1512 1514 1515 1516 1517 1518 1520 1521 1523 1523 1524	иниминавининининимини	ท่ทยทยยยยยยยยยยยยยยยยยยยยยยยยยยยยยยยยยย	P10-20 P10-36 P10-38 P10-138 P10-16 R10-06 R10-28 R10-28 R10-12 R10-28 P02-26 P02-26 P02-32 P02-32 P02-32 P02-34 P02-88 R02-28 R02-28 R02-28	888877777977555665465	<i>©©©™©©©©©©©©©©™™™™™™™™™™™™™™™™™™™™™™™</i>	0.387 0.456 0.491 0.517 0.413 0.554 0.554 0.558 0.253 0.387 0.387 0.391 0.391 0.455 0.440	8.1429 8.1429 8.1429 8.1429 8.1425 8.1425 8.1424 8.1424 8.1424 8.1424 8.1424 8.1426 8.1406 8.1406 8.1406 8.1406

TABLE	2.4 OF	LINE BY L	INE LASER	EXTINCTIO	ON MEASUREM	ENTS FOR CO2	LASER	SOURCE
DATE	TIME	RUN CODE	LASER	LINE ID	MOB GAIN	STAT GAIN	TRANS	EX COEF
16Y77 16Y77 16Y77 16Y77 16Y77 16Y77 16Y77 16Y77 16Y77 16Y77 16Y77	1458 1500 1501 1504 1506 1510 1515 1516 1517 1518 1520 1521 1522	ммимимимимими	សសសសសសសសសសស	P10-20 F10-30 P10-38 \$10-10 R10-34 R10-12 P02-32 P02-14 P02-20 R02-20 R02-28 R02-28 R02-28 R02-20	78887955644848	๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛	0.213 0.259 0.259 0.230 0.297 0.096 0.160 0.163 0.258 0.308 0.301 0.211	0.3029 9.2647 9.237 9.458 9.458 9.3331 9.230 9.230 9.230
17 Y 77 17 Y 77	1451 1501 1504 1508 15135 1529 1535 1552 1557 1607 1611 1612 1627	мымымымымымымы	555555555555555 55	P10-20 P10-38 P10-30 P10-20 P10-12 R10-20 R10-34 P02-32 P02-14 P02-08 R02-08 R02-14 R02-20 P10-20	8098772765558547	587655454MMMMM25	0.208 0.259 0.248 0.210 0.225 0.000 0.305 0.305 0.196 0.308 0.308 0.308 0.273 0.196 0.308	0.307 0.264 0.272 0.305 0.2841 1.491 0.252 0.355 0.319 0.605 0.2227
24Y77 24Y77 24Y77 24Y77 24Y77 24Y77 24Y77 24Y77 24Y77 24Y77 24Y77 24Y77 24Y77 24Y77	1429 1434 1434 1435 1437 1438 1440 1449 1455 1456 1457 1458 1458	вамавамавамама	\$\$\$55555555555	P10-20 P10-30 P10-38 P10-20 P10-10-34 R10-22 R10-12 P02-32 P02-14 P02-08 R02-20 R02-20 R02-20	99999888866655555	55555544BBBQQQQ	0.084 0.098 0.100 0.084 0.091 0.142 0.071 0.130 0.160 0.117 0.151 0.188 0.194 0.178	0.483 0.453 0.485 0.485 0.467 0.381 0.517 0.389 0.369 0.369 0.321 0.338
25Y77 25Y77 25Y77 25Y77 25Y77 25Y77 25Y77 25Y77 25Y77 25Y77 25Y77 25Y77 25Y77 25Y77	859 859 966 969 9114 9117 9117 922 922 922 922 922 922 922	амимимимимимимимимимимимимимимимимимими	ກສຣຕກສຣຣຣຣຣຣຣຣຣຣ	P10-20 P10-30 P10-38 P10-20 P10-38 P10-10 R10-34 R10-12 P02-32 P02-14 P02-08 R02-28 R02-28 R02-28	19028899896665494	668445554881 <i>aaaa</i>	0.063 0.071 0.077 0.099 0.115 0.108 0.176 0.196 0.140 0.167 0.181 0.237 0.228	0.539 9.515 9.501 9.451 9.422 9.435 9.339 9.642 9.318 9.350 9.334 9.350 9.334

Table 3.1. Aerosol extinction coefficients derived on the basis of contrast attenuation measurements at the Cape Canaveral shore (see Fig. 3.1 for path definition).

4	6 mt 41						en derinit	
JATE	1 2 4	MAY	E CETTALTEN					
		THE LENG	THE FRANCE	1				
		(KM) (MICH		DATE	L ተር a			
41 MAH	77 1500		⁽⁷⁸⁾	*****	71=	t LENGTH	MAVE EXTENC	114
11 MAR	!! 1550	.OH 0.40.	۱۸ A			401 14		
IL MAN	2 86	,. OH D. 404		12 Max	• •	``-,	CHICHON) CAN	
31 MAH	?? 1940	1004 0.414	4 7,778	12 MAR	100	1.08		
II MAR		7.00 0.440	_ ~,,,,	12 Man	110	-08	0.4050 0.1	7.4
31 MAN	1504	7.0# O.4##		12 MAH			0.11	**
11 MAR	1520	**** 0.505	× • • • • • • • • • • • • • • • • • • •	47 Man	?? 104#	-08	0.4 148 0.16	
11 HAM	1342	** OH 0.414	40.748	17 MAR			0.4500 0.17	
11 MAN 1	1 107	OH 0.420	0.244	17 RAN		' • V II	0.4480 0.10	
ll mam :		1.08 0.144		17 MAR			V.7050 A	
II MAN)	,	-ON 0-1776	*****	12 MAR	1014	4.01		
ll man ,	, ,,,,	-OH 0.1846	44541	12 MAN 7	1039	5.0x	0.4100	
11 mam /	1324	0.4000	0.118	17 MAR 7	7	. • O M	* * * * * * * * * * * * * * * * * * * *	
11 MAH 7		A A		17 MAR 7	1	7 · O #	1.4240	
11 MAR)			0.161	17 MAR 7		7408	1 444. *******	
11 mam 7	1779		V • 10 /	12 MAR 7		3.00	1.4660	
11 Ham y	4348	440.54	0.281	27 46H 7	, ,,,,,	7~87# (1. A 300	
11 MAR /	1,00		0.171	17 PAR 7		, · 64 (****	
11 man	1417		0.411	12 MAH 71		7.08 0		
11 Man 17	1540		0.411	12 440		0 MO+1	ADA VOLEU	
11 MAH 77	1504	> Y47700	0.420	12 HAR 11	1007	1.08 7	A 84 3	
32 MAR 77	1520	, , , , , , , , , , , , , , , , , , , ,	0.108	17 MAH 73	-007	2.51		
	1542		0.40#	17 MAW 77		2.42 6	4040	
	1507		0. 176	12 MAH))	1011	7.47 0		
	1574	2.57 0.5200	0. 176	12 PAR 77	104#	3 4 5	44.00	
	1144	V.7461	0. 19#	17 MAR ri	1010			
	1510	3.47 0.4770	0. 194	12 MAH 77	1016		1010 0.144	
41 MAH 77	1529	D-4896	0.198	12 MAG 11	1042		1145 0.204	
11 MAN 17	1518	2.47 0.4000	0.404	17 MAN	1014		0.704	
il man yy	1514	[*] 0. A200		17 MAR 71	1019		300 0.154	
11 MAH 77	144-	P.ALZA	0.470 9.198	12 Man .	1044	,	441 0.719	
33 MAN 17		C+11 C- 120	0.41	12 MAN 11	1011	,	770 0.247	
31 MAH 77	1500	7.37 7.6941		12 man);	1041		MV6 5	
11 Man 11	2444	1.28 0.40.0	0-626	12 PAR 17	1044		000 0.73	
II TAN TY	141.	0.4010	0.649	12 MAR 17	1020			
11 MAW 77	1140	'*** 0.434a	0.654	12 MAN 77	1100	, , ,		
EE MAR 77	1404	-28 0.490		12 MAH -7	1047		128 0 144	
II MAR 77	1430	*** 0.4980	0.641	12 MAR 77	1110		** 1	
11 MAH 77	154.	· 74 0.5050	0.607		1007		4	
11 MAR 77	1444	. 28 0.4144	0.678	17 MAN 17	1101		950 0.34 m	
41 748 17	34.54	• 28 O. 5300	0.478	17 MAR 11			30 0 111	
II MAN 17	1444	-28 D.44A1	0.424				38 0.224	
II FAN 77	1414	28 0.5726	0.641		1010	0.44	00 0 144	
11 -40	1310	CB 0. 4864	0.647			0.48	BO 0.334	
11 MAN 77	1529	TH C.ADAA	0.424		144.	0.50	0.734	
li man ,,	14.1	2 N Q A200	0-607		1011	0.51	0	
11 MAN 11	1314	" 0.4444	0.647		1030	0.17	0 0 44	
II MAN 17	150 1	·	0.441		1044	0.146	1 0.344	
•	1948 i.	8 0.40	7.748	17 MAR 77	1011	1(1 0.577	0 0.300	
			.041	70.77	1041	0.184	0.279	
					1044			
					1010	0.620	V *** ***	
						78 0.633	4.1.46	
					104. '*	78 D. A 121		
						2# O.694	V•246	
				•		'H 0.694	0.101	
							0.740	

Table 3.1 (continued)

DATE	Laca MIT		MAVE	EXTINCTION					
			LENGTH	. V. TAC 114M		_			
		(KH) (PICPON		DATE	4.0	CAL PA	TM	
14 MAR	>>			? (/KM)	0416	T			EXTINCTION
14 MAR	841	7 5.08						· · · · · · · · · · · · · · · · · · ·	T CAPP-
14 74	77 931		0.4050	0.144			CK	(HICROI	
14 HAR	,,	7405	0.4050		14 HAR	77			1) (/K#)
14 MAR	// ei-	7.08	Ú++ 35#	0.149	14 MAR	••	25 5.8		
14 HAR	· · · · · ·	` .DE	2.4500	0.136	14 HAR	<u>''</u> 16	02 5.0	424030	
14 MAR	(* 152			0.140	17 748	77	4.0		0.153
14 44	910		-4880	0-114	14 HAR	77			
14 MAR	7	7000 (-5050	0.121	14 MAN	77		8 0.4500	0.144
14 MAR 7	7:	5.08	1.5145		14 MAR	**			0.145
14 MAR 7	7 856		-5200	0.125	14 MAN	. 17	42 s.a	444000	0.125
14 MAR 7	, 717	5-08	200	0-114	14	<u>"</u> 15			0.118
14 ***	475		.5461	0.171	14 MAN	J7 9# ·			0.118
14 MAR 7	7 900		.5770	0.133	14 HAR	77 154		0.5200	
14 MAN 7	,	5-08 0	+5896		14 MAR :	"		0.5461	9-118
14 TAR 7	, 787	5-08 n	6000	0-129	14 MAR Y	[[159	5.08		0.175
14 MAR 77	, 717			0-136	14 MAH 7	153	5.08	907170	0.125
HAR T	703		6200	0.125	14 849 7	7 140	,	447030	0.162
			6328	0.121	, ,	7 184	, ,,,,	0-5896	
14 MAH 77	914		6328	0-140	14 MAR 7	7 144	_ '4V8	0.4000	0.162
14 MAR 77		J-98 G.	6943		14 MAR Y			0.6200	0.153
14 MAR 77	7.78		6943	0.155	14 MAR 7	,,	5.00		0.149
14 MAN 77	847			0.157		1400		0-6328	0.162
14 HAR 77	930		4050	0.150			,. ve	0.6943	0.176
14	707	3 4 5	4050	0.162	14 MAR TI	1650	/•V8	0.6943	
14 MAN 77	920		4358	0.150	14 MAR 77			0-4050	9-207
14 MAR 77		2.57 0.	45C0		14 MAN 77			0-4050	0-192
14 MAR 77	852	2.57 0.	1880	9-156	14 MAR 77	1540	2.57	0.4070	0.186
14 MAR 77	710	2.57 0 4	1990	0.133	14 MAR 77	1552		0.4358	0.192
	\$22		050	0.150		1579	2.57	0-4500	0-192
	856		145	6.150	14 MAR 77	1542	2.57	0.4880	
14 RAR /7	912	2.57 0.5	200	0.139	14 HAR 77		2.57	0.5050	0.212
14 MAR 77		(*)/ 0.5	461		14 MAH 77	1555	2.57		0.128
14 MAR 77	925	2.47 0.5	770	0.150	14 MAR 77	1532	2.57	0.5145	0.112
14 MAP 77	700	2.57 0.6		0.174	24 242	1545	2.57	0.5200	0.150
14 HAR 77	715		4.26	0.156	14 MAR 77	1557		0-5461	0.150
77 77	917	3	700	0.140	14 MAN 77		2.51	0.5770	
14 HAR 77	903	2.57 0.4		0.168	14 MAR 77	1534	2.57	0.5896	0-156
14 HAR 77		2.57 0.4			14 MAR YY	1605	2.57	7 5000	0.199
14 MAR 77	934	2.57 0.6	4.5	0.162	14 MAR 77	1547	2.57	0.5896	0.192
14 MAH 77	928			0.174	14 848 22	1548	2.57	0.6000	0.205
14 MAN 77	937			0.205		15 37		0.6200	0.199
17 TAR 77	847		43 6	1.212	14 MAR 77	1600	2.57	0.6328	
14 HAR TY	770	1.28 0.40			14 MAR 77		2.58	0.6943	0.226
14 MAR 77		1-78 0.40		-174	14 MAH 77	1607	2.57	0.4044	0.186
14 HAR 77	907	1.28 0.43	•	-174	14 MAR 77	1525		0.6943	0.247
14 HAH 77				-165	TAN 77	1601		U-4050	0.279
14 840)0 n	-165	14 MAR 77	1540	1-28		0.312
14 HAR 77	***	1-28 0.47		-136	14 MAR 77		1.28	* 4 ***	
14 MAR 77		**** 0.504	_		14 MAR 77	1552			- 302
14 MAR 77		-28 0.514		-146	14 MAR 77	1579).373
14 MAR 77	854	-28 0.520		.146	14 HAR 77	1542	1 24	-4880	-214
14 MAH 77			y 0.	177		1555	1 1 1	1+>050 a	-214
14 man 77		40,740	I D.	136	14 MAR /7	1532	1.58		-165
14 MAR 77	004	.28 0.577	θ 6.	150	14 RAN 77		58 0	6 44.5	
14 HAR 77	41.	·28 0.589			14 MAR TT	1545		6444	-155
24 MAK 77		-28 0-600		134	14 MAH 77	1551		-5461 0	-214
14 HAR TT	717 1	1-		146		1534	1 14 .	***** O.	-225
14 840				136	14 MAR 77	1547	1-28 0		
14 MAN 77	434			174	14 MAR 77			AAAA	267
14 HAR 77	410	·Z# 0.632#			14 PAR 77	1548		4100	279
14 MAR 77		78 0.694	V-1	174	14 MAN 77	1537		6500 0.	325
••		,,	***	155	14 840	1606	1 34	.0 AZE	279
		0.6443	٠.	45	14 RAR 17	1400		6328 A.	267
			-		14 PAR 77	140.	3-20 0.		
					•	1406		6743	214
									257

Table 3.1.(continued)

	LaCAL	PATH	WAVE	EXTINCTION					
DATE	TIPE	LENGTH		COEFF.		LOCAL	PATH	WAVE	EXTINCTION
		(KH)	(MICRON)	(/K#)	DATE	TIME	LENGTH	LENGTH	COEFF.
		,,,,	((/k=)			(K#)	(MICRON)	
1 APR 77	948	5.08	0.4050	0.373	3 445 45				
1 APP 77	1031	5.08	0.4050	0.361	2 APR 77 2 APR 77	8 39	5.08	0.4050	0.214
1 APR 77	1005	5.08	0.4358	0.327		924	5.08	0.4050	0.214
1 APK 77	1018	5.08	0.4500	0.307		858	5.08	0-4359	0-192
1 APR 77	953	5.08	0.4880	0.255	2 APK 77	914	5.08	0.4500	0.192
1 APK 77	1006	5.08	1-5050	0.273	? APR 77 2 APR 77	843	5.08	0.4888	0.158
1 APK 77	1021	5.08	J-5145	0.265		100	5.08	0.5950	0.163
1 APR 77	955	5.08	0.5200	0.281	2 APR 77 2 APR 77	917	5.08	0.5145	0.158
1 APK 77	1018	5.00	0.5461	0.237		844	5.08	0.5200	0.146
1 APR 77	1023	5.08	0-5770	0.237		904	5.08	0.5461	0.146
1 APP 77	959	5.08	0.5896	0.231	2 APP 77 2 APR 77	919	5.08	0.5770	0.146
1 APR 77	1013	5.08	0.6000	0.244		850	5.08	0.5896	0.130
1 APR 77	1015	5.08	0-6290	0.207		907	5.08	0.4000	0.134
1 APH 77	1002	5.00	0.6328	0.201	2 APP 77 2 APK 77	911	5.08	0.6200	0.134
1 APR 77	1036	5.08	0.6328	0.218		854	5.08	0.6328	0.123
1 APR 77	1927	5-08	0-6943	0.218	2 APK 77 2 APR 77	928	5.08	0.6328	0.130
1 APR 77	1037	5.08	0.6943	0-218	2 APH 77	922	5-08	0.6743	0-134
1 APR 77	748	2.57	0.4050	0.408	2 APR 77	930	5.08	0.6943	0.138
1 APR 77	1032	2-57	0.4050	0.408		839	2.57	0.4050	0.254
1 APR 77	1005	2.57	0.4358	0.378	2 APR 77 2 APH 77	924	2.57	0.4050	0.254
1 APR 77	1018	2-57	0.4500	0.357	2 APR 77	850	2.57	0.4358	0.233
1 APR 77	953	2.57	0.4860	0.328	2 APR 77	714	2.57	0.4500	0.240
1 APK 77	1000	2.57	0-5050	0.311	2 APH 77	843	2.57	0.4880	0.199
1 APR 77	1021	2.57	0.5145	0.328	2 APR 77	900	2.57	0.5050	0.212
1 APR 77	955	2.57	0.5200	0.302		917	2.57	0.5145	0.205
1 APR 77	1010	2.57	0.5461	0.311	2 APK 77 2 APR 77	846	2.57	0.5200	0.199
1 APR 77	1023	2.57	0.5770	0.319	2 APR 77	904	2.57	0.5461	0.212
1 APR 77	959	2.57	0.5896	0.378	2 APH 77	919	2.57	0.5770	0.212
1 APR 77	1013	2.57	0-4500	0.311	2 APR 77	850	2.57	0.5896	0.205
1 APR 77	1015	2.57	0-6200	0.286	2 APH 77	907	2.57	0-6000	0-219
1 APR 77	1002	2.57	0.6328	0.302	2 APR 77	911	2.57	0.6200	0.177
1 APR 77	1035	2.57	0.6328	0.311	2 APR 77	854	2.57	0.6328	0.199
1 APR 77 1 APR 77	1027	2.57	0-6943	0.311	2 APK 77	928	2.57	0-6328	0.219
1 APR 77 1 APR 77	1036	2.57	0.6943	0.328	2 APR 77	355	2.57	0.6943	0.219
1 APR 77	948	58	0.4050	0.511	Z APR 77	930	2.57	9-4943	0.219
1 APR 77	10%	1.28	0.4050	0.526	2 APR 77	839 858	1.28	0-4051	0.313
1 APR 77	1005	1.28	0.4358	0.496	2 APR 77	914	1.28	0.4358	0.268
1 APR 77	1018	1.20	0.4500	0.453	2 APR 77	843	1.20	0.4500	0.290
1 APR 77	953	1.50	0.4880	0.373	2 APK 77	700	1.28	0.4880	0.225
1 APK 77	1608	1.28	0.5050	0.399	2 APR 77	717		0.5050	0-235
1 APR 77	1021	1.28	0.5145	0.399	2 APH 77	844		0.5145	0.246
	955	1.20	0-5200	0.361	2 APP 77	904		0.5200	0.225
	1010	1.28	0-5461	0.373	2 APR 77	717		0.5461	0-246
1 APR 77	1023	1.28	0.5770	0.386	2 APR 77	850		0-5770	0.246
	959	1.28	0.5896	0.399	2 APR 77	907		0.5896	0.246
	1013	1-28	0.6000	0.399	2 APR 77	911		0-6000	0-246
	1015	1-28	0.6200	0.399	2 APR 77	854		0.4200	0.225
	1002	1.20	0.632R	0.399	2 APR 77	922		0.6328	0.235
	1034	1.28	0 • 6328	0.386				0-6943	0-257
	1077	1.28	0.6943	0.399					
	1039	1.28	0.6943	0.412					

Table 3.1.(continued)

	LOCAL	PATH	WAVE	EXTINCTION				LOCAL	PATH	WAVE	EXTINCTION
DATE	TIME	LENGTH	LENGTH	COEFF.		DATE		TIME	LENGTH	LENGTH	COEFF.
		(KH)	(ATCRON)						(K4)	(HICRON)	(/K#)
			•	• • • •					,	(HICHOR)	(/=-/
4 APR 77	846	5.08	0.4050	0.265	5	APR	17	950	5.08	0.4050	0.209
4 APR 77	927	5.08	0-4050	0.258	5	APP	71	1029	5.08	0.4050	0.212
4 APK 77	905	5.08	0-4358	0.224	5	APR	77	1010	5.08	0.4358	0.185
4 APR 77	918	5.08	0-4500	0-224	5	APK	77	1020	5.08	0.4500	0.196
4 APR 77	849	5.08	0.4880	0.190	5	APR	77	958	5.08	0.4880	0.185
4 APR 77	907	5-08	0-5050	0.190	5	APR	77	1012	5.08	0.5050	0.176
4 APR 77	923	5.08	0-5145	0.190		APH		1022	5.08	0.5145	0.196
4 APK 77	854	5.08	0.5200	0.190	5	APR		1000	5.08	0-5700	0.162
4 APR 77	909	5.08	0.5461	0-176	5	APR		1014	5.08	0.5.51	0.176
4 APK 77	922	5.08	0.5770	0.170		APW	77	1024	5.08	0.57 0	0.196
4 AFK 77	700	5.08	0.5896	0.180	5	APR		1003	5.08	0.589	0.185
4 APR 77	912	5.08	0.6000	0-196	5	APH		1016	5.08	0-6900	0.207
4 APR 77	916	5.08	0.6200	0.171	5	APP		1017	5-08	0-6200	0.185
4 APR 77	903	5.08	0.6328	0.166		APH		1006	5.08	0.6328	0.140
4 APR 77	934	5.08	0-6328	0-176		APH		1034	5.08	0.6328	0-190
4 APK 77	926	5.08	0.6943	0.171	5	APR		1026	5.00	0.6943	0.212
4 APR 77	935	5.08	0.6943	Q-176	5	APR		950	2.57	0.4050	0.352
4 APR 77	846	2.57	0.4050	0-246	5	APR		1028	2.57	0-4050	0-366
4 APR 77	928	2.57	0-4050	0.286	5	APR		1010	2.57	0.435R	0.357
4 APR 77	905	2.57	0.4358	0.286	5	APR		1920	2.57	0.4500	0.347
4 APR 77	918	2.57	0.4500	0.270		APS		958	2.57	0-4880	0-320
	849	2.57	0-4880	0.233	5	APR		1012	7-57	0.5050	0.338
4 APR 77 4 APR 77	907	2.57	0.5050	0-247		APR		1022	2.57	0.5:45	0.408
4 APR TT	920	2.57	0.5145	0.233	5	APR		1000	2.57	0.5200	0.357
4 APR 77	856	2.57	0-5200	0.219	5	APR		1014	2.57	0-5461	0.408
4 APR 77	909	2.57	0.5461	0-240	5			1024	2.57	0.5770	C.431
4 APR 77	922	2.57	0.5770	0.247	5	APR		1003	2.57	0-5896	0.387
4 APR 77	912	2.57 2.57	0.5896 0.600C	0-240	5	APR		1016	2.57	0-6000	0-456
4 APR 77	712	2.57	0.6500	0.240	ś	APR		1017	2.57	0.4200	0.495
4 APR 77	903	2.57	0.6328	0.233	,	APK		1006	2.57	0.6328	0.431
4 APR 77	428	2.57	0.6328	0.233 0.240	5	APP		1026	2.57	0-6943	0.495
4 APR 77	726	2.57	0.6943	0.247	ś	APR		950 1010	1 - 28	0.4050	0.412
4 APR 77	936	2.57	0.6943	012.0	ś	APR			1.20	0.4358	0.325
4 APR 77	846	1.28	0.4050	0.399	ś	APP		1020 958	1.28	0-4500	0.257
4 APR 77	905	1.28	0.4358	0.373	ś	APK		1012	1.78 1.28	0.4880	0.247
4 APR 77	849	1.28	0.4880	0.313	Š	APE		1022		0.5050	0.412
4 APR 77	918	1.28	0.4500	0.361	ś	APR		1000	1-28	0.5145	0.337
4 APR 77	907	1.28	0.5050	0.337		APR		1014	1.28 1.26	3-5200	0.399
4 APR 77	720	1.28	0.5145	0.301	Š	APF		1024		0.5461	0.386
4 APR TT	856	1.78	8-5200	0.279	ś	APK		1003	1.28	0-5770 0-5896	0.279
4 APR 77	909	1.28	0.5461	0.301	ś	APF		1016	1.28		0-439
4 8FH 77	922	1.28	0.5770	0.325	Š	No W		1017	1.26	0.6000	0.481
4 4PR 77	900	1.28	0.5896	0.313	Ś	APH		1006	1.28	0.6200 0.6328	0.361
4 APR 77	912	1.28	0.6000	0.337	ś	APE		1026	1.28		0.349
4 APR 77	914	1.28	0.6200	0.325	•		• •	. 3.20	1.44	0.6943	0.439
4 APR 77	903	1.20	0.6328	0.313							
4 APH 77	926	1.20	0-6943	0.361							

Table 3.1.(continued)

						LHEAL	PATH		MITTHETTEN
			1	TINCTION		TIPE	LENGTH	LENGTH	COFFF.
	LOCAL	PATH		GEFF.	DATE	1176	(KH)	(HICROW)	(\KM)
	TIME	LENGTH		(/K#)			(n.)		
DATE		(K#) (HICHON)	(14-1			5.08	0.4050	0.207
					13 MAY 77	917	5.08	0.4050	0.231
	750	5.08	0.4050	0.162	13 MAY 77	1023	5.06	0.4500	0.140
APR 77	835	5.08	0.4050	0.162	13 HAY 77	1001		6.4880	0.136
APR 77	812	5.08	0.4358	0.121	13 MAY 77	922	5.08	0.4880	0.166
APK 77	124	5.08	0.4500	0-125	13 MAY 77	1024	5.08	0.5050	0.153
6 APR 77		5.08	0.4880	0.114	13 MAY 77	946	5.08	9.5145	0.144
6 APH 77	753	5.08	0.5050	0.101	13 RAY 77	1005	5.08	0.5709	0.171
6 APR 77	808	5.08	0.5145	0.107	13 NAY 77	930	5.08	0.5461	0.133
4 APR 77	928	5.00	0.5200	0.101	13 MAY 77	951	5.08		0.125
6 APH TT	758	5.08	0.5461	0.114	13 HAY 77	1012	5.08		0.125
6 APR 77	815	5.08	0.5770	0.101	13 MAY 77	935	5.08		0.133
6 APR 77	630		0.5996	0.101	13 MAY 77	954	5.08	0.6000	0.125
6 APK 77	800	5.08	0.6000	0.111	13 RAY ??	958	5.08		0.107
6 APR 77	817	5.08	0.6200	0.104	13 RAY 77	938	5.01	0.6328	
6 APR 77	871	5.06	0.6328	0.091		943	5.00	9.4356	
6 APR 77	804	5.08		0.104	13 HAY TT	1014	5.01	0.6500	
6 APR 77	833	5.08	Q-6943	0.162	13 MAY 77	1012	5.0	0.6943	0-121
4 APH 77	750	2.57	0.4050	0.156	13 HAY 77	917	2.5	7 0.4050	0.286
6 APR 77	8`>	2.57	0.4050	0.144	13 MAY 77	1022	2.5		0.286
6 APR 77	812	7.57	0.4358	0.139	13 HAY 77		2.5		0.212
	824	2.57	0.4500	0.128	13 RAY 77	943	2.5	7 0.459	0.240
	753	2.57	0.4880		13 MAY 77	1001	2.5		0.212
	808	2,57	0.5050	0.128	13 HAY 77	922	2.5		0 0.22
6 APR 77	828	2.57	0.5145	0.117	13 HAY 77	1026	2.5		0 0.212
6 APR 77	758	2.57	0.5200	0.117	13 HAY ??	946			4 0-212
6 APR 77	915	2.57	0.5461	0.133	13 MAY 77	1005	2.		
6 APR 77	830	2.57		0.128	13 MAY 77	930	2.	,, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	1 0-174
6 APP 77			0.5896	0.128	13 MAY 77	951	2.		10 0-174
6 APR 77				0.139	13 HAY 77	1006		,,	
6 APR 77				0.117	13 HAY 77	9 35	-		
6 APR 77				0.128	13 MAY 71	954			0.168
6 APH 71				0.144	13 MAY 71				
6 479 7				0.240	13 HAY 71	931		57 (2	
6 APR 7				0.279	13 HAY 7	101		57 (.27	
6 APH 3				0.214	13 HAY T				
6 APR T		•		0.20	13 HAY 7	7 91		28 0.40	
6 APR 7				0.174	13 MAY 7			28 0.40	
& APK T		•		0.174	13 HAT T	7 94	3 1	.28 0-43	
6 APP T				0.165	13 HAY 7		1 1	.28 9-45	2 270
6 APH T	7 82				13 MAY 1	7 92	2 1	.28 0.40	
6 APP 1	75				19 787	•		.28 0.4	A 326
	77 81	5 1.		•	13 HAY 1			.28 0.5	
	77 8	30 L-			13 MAY 1			.28 0.5	17/
	77			- 4-4	13 HAY			_78 0.5	200 9-24
		19 1.			13 HAY			.78 0.5	461 0-21
6 APK			28 0-626		13 MAY	• •		.28 0-5	496 Q-ZO
6 APP	• •	04 1-	28 0.63		17 """	• •	,,	.78 0.5	770 0-14
	••		28 0.69	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	12 -41		V-	1.28 0.4	7000 0.SS
6 MAH	••	'			13 MAY	••	, •		200 0-18
					13 FAY	. ,	,,,	• • • •	. 228 0.16
					13 #47	77 9			500 0-30
					13 #87	77 10			6943 0.31
					į3 MAY	77 10	12	1.28 0-	

Table 3.1.(continued)

DATE	LACEL TIPE	PATH MAT LENCTH LENI CKM) (MIC		DATE	LUCAL	PATH LENGTH (KW)	WAYE E LENGTH (MICRON)
14 MAY 77	757	5.08 0.4	050 0.573	14 PAY 77	913	2.57	0.6500
14 MAY 77	805	5.08 0.4		14 MAY 77	711	2.57	0-6943
14 MAY 77	# 30	5.08 0.4		14 MAY 77	752	1.28	0-4050
14 MAY 77	842	5.08 0.4		14 MAY 77	805	1.28	0.4050
14 #47 77	915	5.08 O.4		14 MAY 77	630	1.28	0.4050
14 MAY 77	853	5.08 0.4		14 PAY 77	942 913	1-28	0.4050 0.4050
14 MAY 77	904 844	5.08 0.4 5.08 8.4		14 MAY 77	853	1.26	0.4358
14 MAY 77	752	5.08 0.5		14 MAY 77	904	1.28	0.4500
14 RAY 77	805	5-08 0-5		14 MAY 77	844	1.24	0.4880
14 HAY 77	# 10	5.08 0.5		14 MAY 77	752	1.28	0.5050
14 MAY 77	855	4.08 0.5	050 0.26 5	14 MAY 77	#05	1.24	0.5050
14 MAY 77	904	5.08 0.5		14 MAY 77	634	1.74	0.5050
14 PAY 77	846	5.00 0.5		14 487 77	855	1.28	0.5050
14 #44 77	858	5.98 0.5		14 PAY 77 14 PAY 77	904	1.20	0.5145 0.5200
14 MAY 77	908 848	5.08 0.5		14 PAY 77	846 858	1.28	0.5461
14 MAY 77	900		000 0.185	14 MAY 77	904	1.24	0.5770
14 MAY 77	902		200 0.166	14 PAY 77	848	1.20	0.5896
14 #47 77	758		324 0.251	14 MAT 77	900	1-28	0.4000
14 PAT 77	611		178 0.274	14 MAY 77	902	1-74	4.6700
14 #47 77	636		328 0.196	14 MAY 77	750	1.20	0.6328
14 MAY 77	651		328 0.190	14 MAY 77	811	t-28	0.6324
14 747 77	916		328 0.166	14 MAY 77 14 MAY 77	#36	1.78	0.6328
14 MAY 77	80 3		400 Q.244 400 Q.224	14 MAY 77	851 917	1.28	0.6328
14 PAY 77	#11 #7#		500 0.224 500 0.190	14 PAT 77	#03	1.20	0.6500
14 PAY 77	913		400 4.157	19 MAY 77	•11	1-70	0.6500
14 MAY 77	*11		941 0.162	16 MAY 37	8 7 8	1.20	0.4500
14 PAY 77	752		950 0.5 5	14 MAY 77	913	1-28	0.4500
14 MAY 77	805	2.47 0.4	450 4.441	14 "47 77	911	1.28	0.694 1
. 14 MAY 77	9,0		050 0.44				
14 #47 77	842		050 0.411				
14 MAY 77	414		050 0.357				
14 #67 77	1853 904		1158 0.357 1500 0.319				
14 PAY 77	844		880 0.302				
14 MAY 77	152		050 0.376				
14 PAY 77	805		050 0.330				
24 MPY 77	834		5050 0.302				
24 PAY 77	855		050 9-270				
14 MAY 77	906		145 0.224				
14 #47 77	\$46		5200 0.270 5461 0.233				
14 PAY 77	978 809		770 4.199				
14 MAY 77	846		165.0 408				
14 887 77	760		.000 0.199				
14 MAY 77	902		P500 0-145				
14 PAY 77	758		6728 Q.242				
14 867 77	411		632R 0.226				
14 PSY 77	#34		129 0.219				
14 MAY 77	851		6329 0.199 6328 0.196				
14 747 77	916 803		6500 0.247				
14 847 77	811		6500 0-219				
14 *43 77	816		4500 3-205				
		••••					

Table 3.1. (continued)

	LOCAL	PATH	WAVE	EXTINCTION		LOCAL	PATH	WAVE 6	XTINCTEON .
DATE	TIME	LENGTH	LENGTH	COFFF.	DAIL	TIME	LENGTH	LENGTH	COEFF.
		(K#)	(MICRON)	(/K#)			CKM)	(HICRON)	(/K#)
14 MAY 77	933	5.00	0.4050	0.336	16 MAY 77	1041	5.08	0.4050	0.258
14 MAY 77	1000	5.08	0.4050	0.317	16 MAY 77	1055	5.08	0.4358	0.231
14 MAY 77	744	5.08	0.4358	0.207	16 MAY 77	1107	5.08	0.4500	0.231
14 MAY 77	952	5.08	0.4500	0.265	16 HAY 77	1044	5.08	0.4881	0.201
14 MAY 77	936	5.08	0.4880	0.196	16 MAY 77	1058	5.C0	0.5050	0.185
14 MAY 77	945	5.00	0.5050	0-218	16 MAY 77	1110	5.08	0.5145	0.190
14 MAY 77	954	5.08	0.5145	0.212	16 MAY 77	1046	5.08	0.5200	0.166
14 MAY 77	936	5.08	0.5200	0.207	16 MAY 77	1100	5.08	0.5461	0.171
14 MAY 77	947	5-08	0.5461	0-185	16 MAY 77	1112	5.08	0.5770	0.165
14 TAY 77	956	5.08	0.5770	0.100	16 MAY 77	1049	5.08	0.5896	0.162
14 MAY 77	940	5.08	0.5896	0-166	16 PAY 77	1103			
14 MAY 77	949	5.08	0.6000	0.162	16 PAY 27	1105	5.08	0.6000	0.153
14 PAY 77	951	5.00	0.6200	0.153	16 MAY 77	1052	5.08	0.6200	0.144
14 MAY 77	942	5.08	0.4325	0.153	16 MAY 77	1117	5.08	0.6328	0.136
14 MAY 77	1005	5.08	0.6325	0.153	16 844 77	1115	5.08	0.6500	0.149
14 MAY 77	1000	5.08	0.6500	0.153	16 MAY 77	1041	5.08	0.6943	0.153
14 MAY 77	958	5.08	0.6943	0.144	16 PAT 77	1121	7.57 2.57		0.311
14 PAY 77	933	2.57	0.4050	0.607	16 MAY 77	1055	2.57	0.4050 0.4358	0.311 0.278
14 MAY 77	1002	2.57	0.4050	0.386	16 PAY 77	1107		0.4500	
14 HAY 77	944	2.57	0.4358	0.311	16 RAY 77	1044	2.57		0.278
14 RAY 77	952	2.57	0.4500	0.328	16 FAY 77		2.57	0.4880	0.240
14 MAY 77	936	2.57	0.4780	0-247	16 MAY 77	105#	7.57	0.5050	0.240
14 PAY 77	945	2.57	0.5050	0.270	16 PAY 77	1110 1046	2.57	0.5145	0.233
14 PAY 77	954	2.57	0.5145	0.247	16 PAY 77	1100	2.57 2.57	0.5200 0.5461	0.219 0.226
14 MAY 77	938	2.57	0.5700	0-236	16 PAY 77	1112	2.57	0.5770	
14 MAY 77	947	2.57	0.5461	0.226	16 MAY 77	1049	2.57	0.5896	0-226 0-219
14 MAY 77	956	2.57	0.5770	0.240	16 MAY 77	1103	2.57	0.6000	0.226
14 MAY 77	740	2.57	0.5896	0.199	16 WAY 77	1105	2.57	0.6200	0.199
14 MAY 77	949	2.57	0.6000	0.219	16 MAY 77	1052	2.57	0.6328	0.199
14 PAY 77	951	2.57	0.6200	0.219	16 MAY 77	1117	2.57	0.6500	0.212
14 MAY 77	942	2.57	0.6328	0.174	16 MAY 77	1115	2.57	0.6943	0.212
14 MAY 77	1004	2.57	0.6329	0.229	16 MAY 77	1124	2.57	0.6943	0.217
14 MAY 77	1000	7.57	0.6500	0.212	16 MAY 77	1041	1.28	0.4050	0.386
14 MAY 77	958	2.57	0.6943	0.233	16 MAY 77	1121	1.28	0.4050	0.399
14 MAY 77	933	1.28	0.4050	0.399	16 PAY 77	1055	1.28	0.4358	0.349
14 HAY 77	100	1.20	0.4050	0.439	16 MAY 77	1107	1.28	0.4500	0.349
14 RAY 77	944	1.28	0.4358	0.337	16 MAY 77	1044	1.28	0.4880	0.301
14 HAY 77	952	1.28	0.4500	0.325	16 MAY 77	1058	1.28	0.5050	0.301
14 PAY 77	936	1.28	0.4850	0.279	16 PAY 77	1110	1.28	0.5145	0.279
14 HAY 77	945	1.28	0.5050	0.301	16 MAY 77	1046	1.78	0.5200	0.290
14 MAY 77	954	1.28	0.5145	0.246	16 MAY 77	1100	1.20	0.5461	0.268
14 MAY 77	738	1.26	0.5200	0.246	16 MAY 77	1112	1.28	0.5770	0.268
14 RAY 77	947	1.28	0.5461	0.235	16 MAY 77	1049	1.28	0.5196	0.257
14 MAY 77	954	1.28	0.5770	0.235	16 MAY 77	1103	1.28	0.6000	0.257
14 PAY 77	140	1.20	0.5#96	0.225	16 PAY 77	1105	1.28	0.6200	0.246
14 MAY 77	949	1.28	0.6000	0.225	16 MAY 77	1052	1.20	0.6329	0.257
14 MAY 77	951	1.28	0.6700	0.214	16 FAY 77	1117	1.28	0.6500	0.268
14 RAY 77	942	1.28	0.6328	0.204	16 MAY 77	1115	1.75	0.6943	0.301
14 MAY 77	1005	1.28	0.6328	9.325	16 MAY 77	1125	1.70	0.6941	0.301
14 HAY 77	1000	1.28	0.6500	0.268	•• •• ••	,	1000	V . W - 7 1	44,701
14 PAY 77	958	1.26	0.6943	0.268					
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Table 3.1.(continued)

	LOCAL	PATH	WAVE	FXTINCTION					
DATE	TIPE	LENGTH				LOCAL	PATH	WAVE	EXTINCTION
		(KH)	(MICPON)	COEFF.	DATE	1 I mt	LENGTH	LENGTH	COFFF.
			(-10-04)	(/KM)			(KM)	(RICRON)	(/K#)
16 MAY 77	1210	5.06	0.4050						*****
16 ALT 77	1247	5.08	0.4050	0.273	17 MAY 77	1221	5.06	0.4050	0.417
16 MAY 77	1271	5-08		0.258	17 MAY 77	1255	5.08	0-4050	0.402
16 PAY 77	1232	5-08	0-4358	0.244	17 MAY 77	1232	5.00	0.4350	0.361
16 HAY 77	1212	5.08	0-4500	0-231	17 MAY 77	1243	5.05	0.4560	0-361
16 PAY 77	1223	5.08	0.4880	0.201	17 MAY 77	1023	5.08	0.4880	0.327
16 FAT 77	1235		9.5050	0-196	17 MAY 77	1234	5.08	0.5050	0.327
16 MAY 77	1214	5-08	0-5145	0-190	17 MAY 77	1245	5.06	0.5145	0.307
16 HAY 77	1276	5.08	0.5200	0-196	17 MAY 27	1025	5.08	0.5200	0.317
16 PAY 77	1237	5.08	0.5461	0-170	17 MAY 27	1236	4.08	0.5461	0.298
16 MAY 77	1216	5-06	0-5770	0-196	IT MAY 77	1248	5.08	0.5770	0.289
16 MAY 77	1228	5-08	0-5896	0.176	17 FAT 77	1027	5.08	0-5896	0.289
16 PAY 77		5.08	0-6000	0.1*0	17 MAY 77	1238	5.08	0.6000	
16 PAY 77	1230	5-08	0-6500	0-176	LT #41 77	1241	5.88	9.6200	0-289
16 MAY 77	1218	5.08	0.6328	9.176	17 MAY 77	1229	5.08	0.6328	0.265
16 PAY 77	1247	5-08	0.6328	0.180	17 447 77	1252	5.08		0-265
16 FAY 77	1242	5.08	9-6500	0.176	17 MAY 77	1250	5.08	0-6500	0.273
16 HAY 77	1240	5.08	0.6943	9-196	17 MAY 77	1221	2.57	0.6943	0.289
16 MAY 77	1210	2.57	9.4050	0.328	17 MAY 77	1255	2.57		0.524
16 WAY 77	1246	2.57	0-4050	0.311	17 MAY 77	1232	2.57	0-4050	0.468
16 MAY 77	1221	2.57	0.4358	0-311	17 MAY 77	1243		0.4358	0.468
16 PAY 77	1232	2.57	0.4500	0.302	17 MAY TT	1223	2.57	0.4500	0.450
16 MAY 77	1212	2.57	0.4680	20562	17 MAY 77	1274	2.57	0.4860	0-420
	1223	2.57	0.5050	0.276	17 MAY 77	1245	2.57	0.5050	0.470
16 MAY 77	1235	2.57	0.5145	0-270	17 MAY 77	1225	2.57	0.5145	0.408
16 MAY 77 16 MAY 77	1214	2.57	0.5200	0.254	17 MAY 77	1236	2.57	0.5200	0.431
	1226	2.57	0.5461	0.278	17 MAY 77	1248	2.57	0.5461	0-420
16 MAY 77	1237	2.57	0.5770	0.276	17 PAY 77	1227	2,57	3.5770	0.398
16 MAY 77	1216	2.57	9.5896	0.262	17 RAY 77	1238	2.57	0.5896	0.431
16 PAY 77	1228	2.57	9-6990	0.278	ST MAY 77	1241	2.57	0.6000	0-420
16 MAY 77	1230	2.57	0-6500	0-247	17 PAY 77	1550	2.57	0.6200	0.387
16 MAY 77	1216	2.57	9-6328	0.247	17 PAY 77		2.57	0.6328	0-408
16 RAY 77	1248	2.57	0.6328	0.262	17 MAY 77	1252	2.57	0-6500	0.387
16 MAY 77	1242	2.57	9-6943	0.270	17 PAY 77	1250 1221	2.57	0.6943	0.39#
16 MAY 77	1210	1-28	0.4050	0.399	17 #AY 17		1.28	0.4050	0.659
16 MAY 77	1245	1.28	0.4050	0.412	17 #AY 77	1254	1.28	0-4050	0-641
16 PAY 77	1221	1.28	0.4358	0.386	17 MAY 77	1232	1.78	0.4358	0.641
16 MAY YY	1212	1.28	9-4880	0.325	17 MAY 77	1243	1.28	0.4500	0.557
16 HAY 77	1232	1.28	0.4500	0.386	17 MAY 77	1223	1-26	0.4880	0.573
16 MAY 77	1223	1.24	0.5050	0.337	17 =AY 77	1234	1.76	0.5050	0.526
14 HAY 77	1235	1.28	0.5145	0-313	17 MAY 77	1245	1-28	0.5145	0.511
16 MAY 77	1214	1-28	9.5200	0.301	17 MAY 77	1225	1.28	0.5200	0.526
16 MAY 77	1226	1.28	0.5461	0.325	17 MAY 77	1236	1.78	0.5461	0.511
16 MAY 77	1237	1.24	0.5770	0.325	17 MAY 77	1248	1-28	0.5770	0.494
16 PAT 77	1216	1.28	0.5396	0.313	17 MAY 77	1227		0.5896	0.557
16 MAY 77	1220	1.28	0.6000	0.325		1238		0.4000	0.511
16 HAY 77	1230	1.28	0.6200	0.325		1241		0.6200	0.496
16 MAY 77	1216	1.28	0-6324	0.301	17 MAY 77	1554	1.28	0.6328	0.511
16 MAY 77	1249	1.28	0-6328	0.313	17 #47 77	1250	1-28	0.6943	0.496
16 MAY 77	1242	1.28	0.6500	0.301	17 MAY 77	1252	1.26	0-6500	0-467
16 MAY 77	1240	1.28	0-6943	0.349					•
	-		/	0 0 3 7 7					

Table 3.1. (continued)

	LPCAL	PATH	WAVE I						
DATE	Almé	LENGTH		XTINCTION		LOCAL	PATH	WAVE	EXTINCTION
		(KM)	(HICGON)	tuere.	DATE	7 I PE	LENGTH	LENGTH	COEFF.
		(80)	("I("ON)	(/K#)			(K#)	(MICRON)	
18 HAY 77	1000	5.08	0.4050						
18 MAY 77	1040	5.08	9.4050	0.361	19 MAY 77	1122	<.0B	0.4050	0.417
18 MAT 77	1003	5.08	0-4358	0 • 3 • 1 0 • 3 2 7	19 MAY 77	1220	5.08	0-4050	0.417
18 MAY 77	1005	5.08	0.4500	0.327	19 MAY 77	1139	<.08	0-4358	0.373
18 PAY 77	1007	5.08	0.4880	0.273	19 MAY 77	1207	5.00	0.4500	0.338
18 MAY 77	1010	5.08	0.5000	0.273	19 MAY 77	1125	5-08	0-4880	0.317
18 MAY 77	1012	5.00	0.5145	0-251	19 MAY 77	1141	5.08	0-5050	0.291
IS MAY Y7	1013	5.08	0.5200	0.237	19 MAY 77	1214	5.08	0.5145	0.289
18 MAY 77	1016	5-08	0.5461	0.231	19 MAY 77	1130	5.0R	0.5200	0.273
18 MAY 77	1018	5.08	0.5770	0-196	19 MAY 77	1144	5.08	0-5461	0.265
18 MAY 77	1026	5.00	0.5896	0-196	19 MAY 77	1216	5.08	0-5770	0.265
18 MAY 77	1030	5.08	0.6000	0-145	19 MAY 77	1135	5.08	0.5896	0.237
18 HAY 77	1032	5.08	9-6200	0.190	19 MAY 77	1148	5-08	0.6000	0.251
18 MAY 77	1034	5-06	0.6328	0.196	19 MAY 77 19 MAY 77	1151	5-08	0-6700	0.224
18 MAY 77	1036	5.08	0.6500	0.140	19 #47 77	1135	5.00	0-6328	0.212
18 PAY 77	1030	5-08	0.6943	0.180		1215	5.08	0.4500	0-224
18 MAY 77	1000	2.57	0.4050	0.408		1212	5-08	0-6943	0.231
18 MAY 77	1040	2.57	0.4050	0.431	19 HAY 77 19 HAY 77	1122	2.57	0-4050	0.468
16 PAY 77	1003	2.57	0.4358	0.398	19 MAY 17	1220	2.57	0.4050	0.468
18 MAY 77	1005	2.57	0.4500	0.376	19 MAY 77	1139	2.57	0.435B	0.420
18 PAY 77	1007	2.57	0.4880	0.338	19 MAY 77	1207	2.57	0-4500	0.468
18 MAY 77	1010	2.57	0.5050	0.319	19 #44 77	1125	2.57	0.4880	0.386
18 PAY 77	1012	2.57	0.5145	0.311	19 MAY 77	1141	2.57	0.5050	0.376
18 HAY 77	1013	2.57	0.5200	0.302	19 MAY 77	1218	2.57	0.5145	0.376
18 FAY 77	1016	2.57	0.5461	0.311	19 PAY 77	1130	2.57	0.5200	0 - 35 7
18 MAY 77	1016	2.57	0.5770	0.270	19 PAY 77	1144	2.57	0.5461	0.357
18 HAY 77	1026	2.57	0.5896	0.233	19 PAY 77	1216	2.57	0.5770	0.357
18 MAY 77	1030	2.51	0.6000	0.226	19 MAY 77	1135	2.57	0-5996	0-338
18 MAY 77	1032	2.57	0.6200	0.254	19 MAY 77	1148 1151	2,57	0-6000	0.338
18 MAY 77	10 34	2.57	0.6328	0.262	19 PAY 77	1135	2.57	0.6200	0.302
18 #47 77	1036	2.57	0.4500	0.262	19 #AY 77	1215	2.57	0-6328	0-246
18 WAY .7	1038	2.57	0.6943	0.262	19 MAY /7		2.57	0.6500	0.378
18 MAY 77	1000	1.28	0.4050	0.481	19 MAY T	1212 1122	2.57	0.6943	0.378
18 #AY 77 18 MAY 77	1040	1.28	0.4050	0.467	19 MAY 77	1220	1.28	0.4050	0.607
•	1003	1.28	0.4358	0.481	19 PAY 77	1139	1.28	0.4050	0.641
18 MAY 77 18 MAY 77	1005	1-58	0-4500	0.439	19 HAY 77	1207	1.20	0.4358	0.526
18 MAY 77	1007	1.78	0.4880	0.399	19 MAY 77	1125	1.28	0.4500	0.557
18 PAY 77	1010	1.28	0.5050	9.412	19 MAY 77	1141		0-4880	0-467
18 #47 77	1012	1-28	0.5145	0.386	19 MAY 77	1218	1.28	0.5050	0-453
18 PAY 77	1013	1.28	0.5200	0.439	19 MAY 77	1130	1.78 1.20	0.5145	0.496
18 MAY 77	1016	1.20	0.5461	0.439	19 MAY 77	1144	1.78	0-5200	0.439
18 PAY 77	1018	1.28	0.5770	0.349	19 MAY 77	1216		0.5461	0.439
18 MAY 77	1026	1-26	0-5496	0.337	19 WAY 77	1132	1.28	0.5770	0.467
18 PAY 77	1070	1.78	0.6000	0.279	19 MAY 77	1148		0-5896 0-6000	0.399
18 #47 77	1032	1.28	0.6200	0.325	19 MAY 77	1151		0.6240	0.426
18 MAY 77	1034	1-28	0-6124	0.349	19 MAY 77	1135		0.4328	0.366
18 #AY 77	1036	1.28	0-6500	0.349	19 MAY 77	1215		0.4500	0.373
	1038	1.28	0.6943	0.394	19 #47 77	1212		0.6943	0.439
								0.4)	0-491

Table 3.1. (continued)

		PATH	WAVE E	XTINCTI TH		LOCAL	PATH	WAVE E	XTINCTION
DATE	LTCAL	LFNGTH	LENGTH	COFFF.	DATE	1146	LENGTH	LENGTH	COEFF.
0416	4146	(KM)	(RICEON)	(/K#)			(K#)	(MICRON)	(/KM)
		(,,,	(4)6-047	(,,,,					
20 MAY 22	843	5.08	0.4050	0,349	20 MAY 77	1322	5.08	0.4050	0.241
20 MAY 77	979	5.08	0.4050	0.273	20 444 77	1 355	<.08	0.4050	0.265
20 MAY 77	901	5.08	0.4358	0.265	20 MAY 77	1335	5.08	0.4358	0.258
20 MAY 77	915	5.08	0.4500	0.237	20 MAY 77	1346	5.08	0-4500	0.265
20 PAY 77	847	<.08	0.4880	0.244	20 P4Y 77	1376	5.08	0.4880	0.237
20 MAY 77	930	5.08	0.4880	0.207	20 MAY 77	1327	5.06	9.5050	0.244
20 MAY 77	904	5.08	0.5050	0.218	20 MAY 77	1348	5.08	0.5145	0.237
20 MAY 11	916	5.09	0.5145	0.190	20 MAY 71	1378	<.08	0.5200	0-274
20 PAY 77	852	5.08	0.5200	9.219	26 MAY 17	1339	5.05	0.5461	0.244
20 WAY 77	907	5.08	0.5461	0.185	20 MAY 77	1350	5.08	0.5770	0.251
20 MAY 77	970	5.08	0.5770	0.171	20 MAY 77	1330	<-08	0.5946	0.218
20 PAY 17	855	5.08	0.5896	0.185	20 MAY 77	1341	5-08	0.6000	9.231
20 "AY 77	910	5.08	0.6000	0.171	20 may 77	1343	5.06	0.6700	155.0
20 MAY 77	911	5.08	0.6200	0.149	20 FAY 77	1332	5.08	0.6328	0-274
20 PAY 77	858	5.08	0.6329	0.166	20 FAT 77	1400	5.09	0.6328	0.231
28 MAY 77	858	5.05	0.6324	0.144	20 MAY 77	1341	5.04	0.6943	0.273
20 MAY 77	976	5.08	0.6500	0.140	20 484 77	1322	2.57	0.4050	0.338
20 MAY 77	921	,,,,,	0.6943	0-149	ZO ##Y 77	1356	2.57	0.4050	0.347
20 MAY 77	843		0.4050	0.371	20 MAY 77	1335	2.57	0.4359	0.338
20 PAY 77	928	2.57	0.4050	0.347	26 MAY 77	1 344	7.57	3.4500	0.338
20 MAY 77	901	2.57	0.4358	0.366	20 MAY 77	1326	2.57	0.4580	0.319
20 MAY 77	915	2.57	0.4500	0.347	20 MAY 77	1337	2.57	0.5050	0.311
20 MAY 77	947	2.57	0.4880	0.366	20 FAY 77	1 348	2.57	0.5145	0.311
77 PAN 05	931	7.57	0.4880	0.102	28 PAY 11	1320	2.57	0.5200	0.311
20 MAY 77	904	2.57	0.5050	0.347	20 444 77	1339	2.57	0.5461	0.319
20 44 77	916	2.57	0.5145	0.262	20 MAY 77	1 350	2.57	0.5770	0.319
20 FAY 77	852	2.57	0.5200	0.311	20 MAY 77	1310	2,57	0.5896	0.319
20 PAY 77	907	7.57	0.5461	0.326	20 PAT 77	1341	2.57	0.6000	0.318
20 MAY 77	920	2.57	0.5770	9.242	TY TAM 05	1343	2.57	0.6500	0.311
20 4/4 77	855	2.57	0.5896	0.294	20 MAY 77	1332	2.57	G.6328	0.319
20 PAY 77	910	2.57	0.4000	0.294	20 #AT 77	1 359	2,57	0.6329	0.319
20 MAT 77	911	2.57	0.6200	0.247	20 MAY 77	1351	2.57	0.6943	1000
20 PAY 77	858	2.57	0.6328	0.254	77 YAW 05	1322	1.20	0.4050	0.453
20 MAY 77	915	2.57	0.6728	0.219	20 947 77	1357	1.28	0.4050	0.481
20 MAY 77	976	2.57	0.6500	0.240	20 MAY 37	1 3 3 5	1.28	0.4358	0.453
20 PAT 77	971	2.57	0.6947	0.212	50 MAY 11	1 346	1.28	0.4500	0.467
20 MAY 77	#43	1.20	0.4050	0.467	20 MAY 17	1376	1,28	0.4880	0.412
20 MAY 77	927	1.76	0.4050	0.576	20 MAY 77	1337	1.28	0-5050	0.426
20 MAY 77	901	1.28	0-4358	0.542	20 PAY 17	1 34 8	1.78	0.5145	0.453
20 MAY 77	915	1.28	0.4500	0.481	20 4AY 77	1328	1.78	0.5200	0.379
70 WAY 71	847	1.24	0.4880	0.313	20 PAY 77	1339	1.28	0.5461	0.399
20 MAY 77	933	1.28	6.4880	0.434	77 VAW 05	1 350	1.28	0.5770	0.453
20 MAY 77	904	1.28	0.5050	0.511	20 #AY 77	1310	1.28	0.5896	
20 MAY 77	916	1.78	0.5145	0.476	20 #AY 77	1341	1.28	0.4000	0.467
20 MAY 77	852	1.20	0.5200	0.467	20 MAY 77	1343	1.28	0.6700	0.439
20 WAY 77	907	1.28	0-5461	0.49,	20 PAY 17	1312	1.20	0.4321	0.453
20 MAY 77	770	1.28	9.5770	0.412	20 MAY 77	1358	1.28	0.4328	
20 MAY 77	855	1.28	0.5996	0.4 6	20 PAY 77	51	1.20	0.6943	0.576
20 MAY 77	910	1.78	0.6000	0.496					
20 MAY 77	911	1.78	0-6500	0 +39					
20 PAY 77	858	1.20	0.6328	0.453					
20 MAY 77	934	1.28	0.6328	0.396					
20 MAY 77	926	1.28	0.6500	0.396					
20 MAY 77	971	1.20	0.6943	0.386					

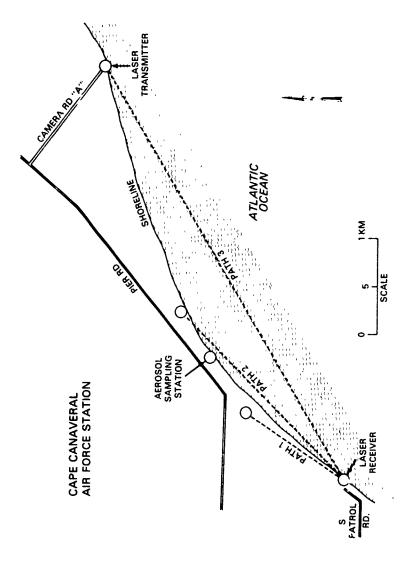
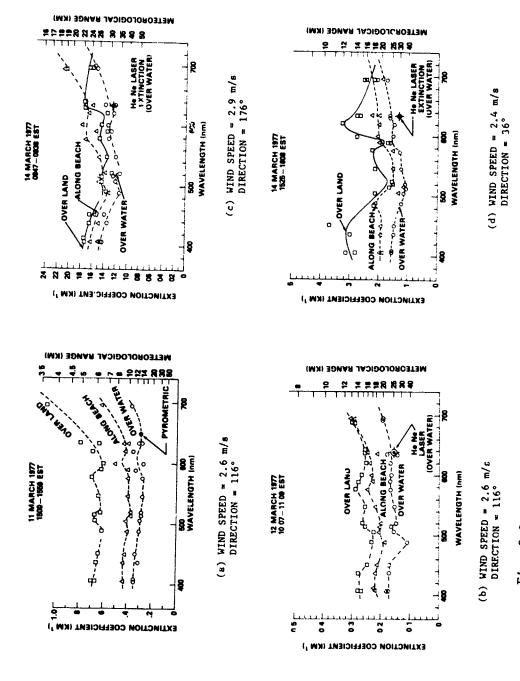
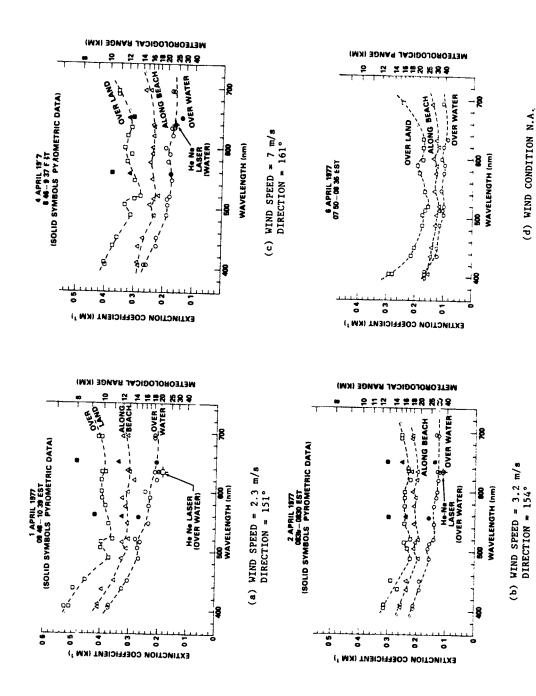


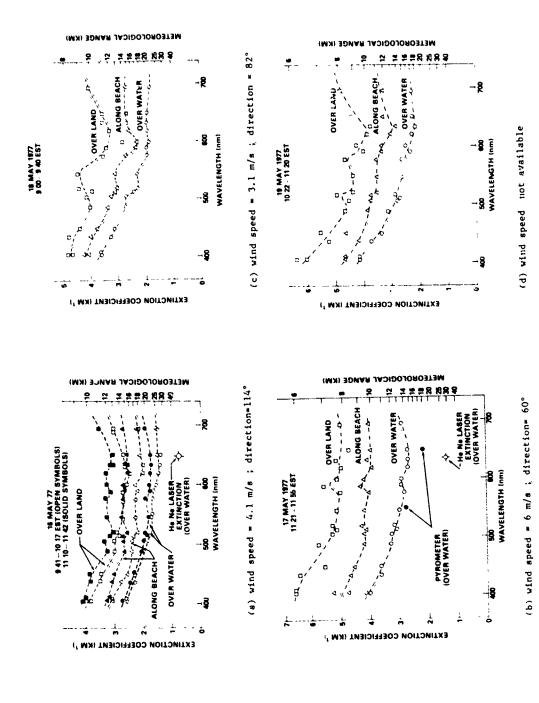
Fig. 3.1. Map of the Cape Canaveral test site showing the three paths utilized for serosol scattering experiments.



AEROSOL EXTINCTION COEFFICIENTS BASED ON CONTRAST MEASUREMENTS ON DISTANT TARGETS AT CAPE CAMAVERAL, FLA DURING MARCH 1977.LASER DATA ARE DERIVED FROM ATTENUATION MEASUREMENTS Fig. 3.2.



AEROSOL EXTINCTION COEFFICIENTS BASED ON CONTRAST MEASUREMENTS AT CAPE CANAVERAL, FLORIDA DURING APRIL 1977.LASER POINTS ARE FROM ATTENUATION DATA. Fig.



1

AEROSOL EXTINCTION COEFFICIENTS BASED IN CONTRAST MEASUREMENTS ON DISTANT TARGET AT CAPE CANAVERAL, FLORIDA DURING MAY 1977, LAS "R DATA ARE DERIVED FROM ATTENUATION MEASUREMENTS. Fig. 3.4.

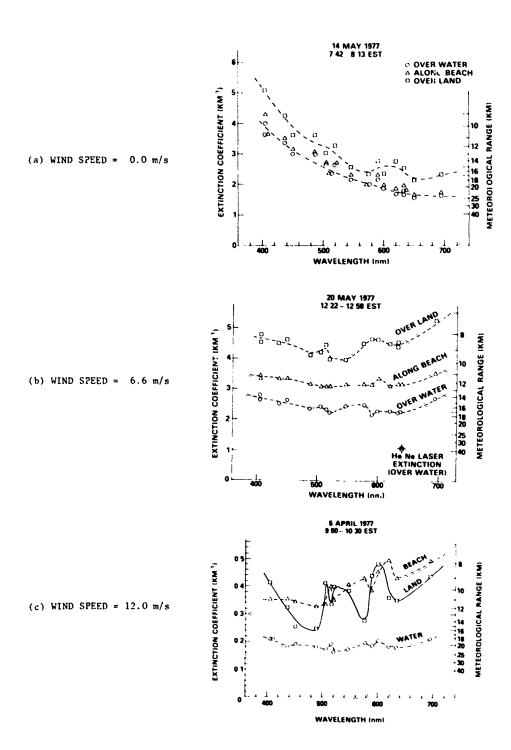


Fig. 3.5. EFFECT OF WIND SPEED ON EXTINCTION COEFFICIENT SPECTRA NEAR THE CAPE CANAVERAL, FLORIDA SHORELINE.

Table 3.2. Aerosol extinction coefficients and visibility derived from pyrometer measurements.

Table 3.2 (Continued)

DATE	LOCAL	RANGE	λ	TRANS-	EXTINC.	VIS.
(y.m.d)	TIME	(km)		ITTANCE	(km ⁻¹)	(km)
22222222233333333333333333333333333333	060200002050215025757050080555510000057002505600003182459004630 01111266668886333460000543144400000570000000001228699911113841325520 11111111111 1111 111 111 111111111111	881107811077110881107711088778877888887878011788888011788888011788810781177871078 5543754377435543774357755777577775555757534755553475347	888888888888888888888888888888888888888	\$\\ 84875386791568\\ 20144173219773331154531998005700738\\ 84875386791568\\ 2014173219773331154531998005700784849331431888\\ 655543654554554531998005700784849331431888\\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	7.218018870491558891876989743914510101822478814 04332700105403588 0.11112011811213114532203114510101822232478814 04332700105403588 0.111120100111213114532203114510101822232478814 04332700105403588 0.1111201000000000000000000000000000000	7626009252547711582907103222780459162593137777399300024884828 223178612170551000860335196864398883275080782166740953460630

Table 3.2 (Continued)

DATE LOCAL RANGE (km) 1 1 1 1 1 1 1 1 1
Color Colo
5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

Table 3.2 (Continued)

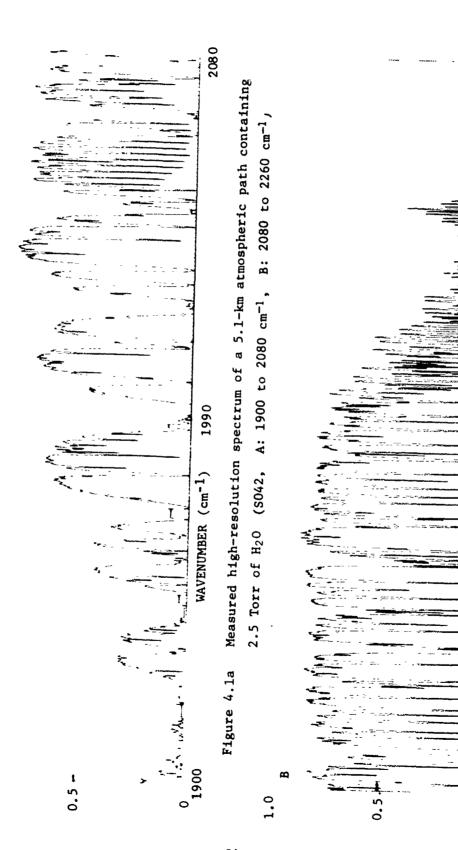
Table 3.2 (Continued)

()	n ⁻¹) (km)
770516 1520 7.47 0.6500 0.359 0.13	
7705223 11445 7.47 0.5568 0.484 0.17 7705224 11325 7.47 0.65508 0.484 0.17 7705224 1335 7.47 0.65508 0.484 0.17 7705224 1335 7.47 0.65508 0.484 0.17 7705224 1335 7.47 0.65508 0.484 0.17 7705224 1335 7.47 0.65508 0.481 1 0.17 7705224 1335 7.47 0.65508 0.481 1 0.17 7705224 1335 7.47 0.65508 0.481 1 0.17 7705224 1335 7.47 0.65508 0.481 1 0.17 7705224 1335 7.47 0.65508 0.481 1 0.17 7705224 1335 7.47 0.65508 0.481 1 0.17 7705224 1335 7.47 0.65508 0.481 1 0.17 7705224 1335 7.47 0.55568 0.481 1 0.17 7705224 1335 7.47 0.47 0.47 0.47 0.47 0.47 0.47 0.47	\$24522736956380738814495050505142902142822 22221112222332222233332231111111112133435664 222211122233222223333223111111112133435664 222217368742770540632323214141251501825876151330

Table 3.2 (Continued)

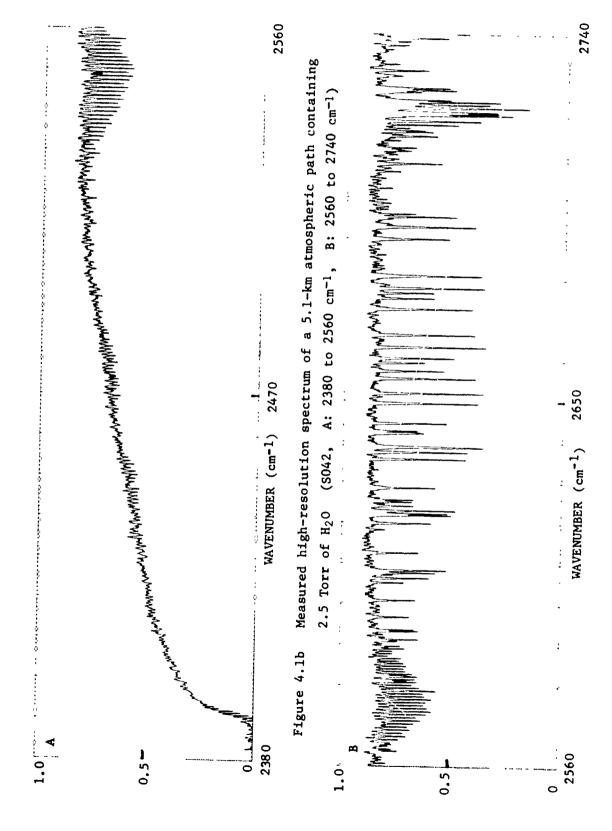
DATE (y.m.d)		RANGI (km)	• • • • • • • • • • • • • • • • • • • •		EXTINC. E (km ⁻¹)	VIS. (km)
770524	1 5 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	7.47 7.47 7.47 7.47 7.47 7.47 7.47 7.47	55680 555555680 00.65555555555556 00.6555555555555555 00.655555555555555555555555555555555555	0.4377753344077959598 0.4375753344077959598	0.238 0.1394 0.1609 0.109 0.135 0.161	3.45.425.185.389.0 11222233222232

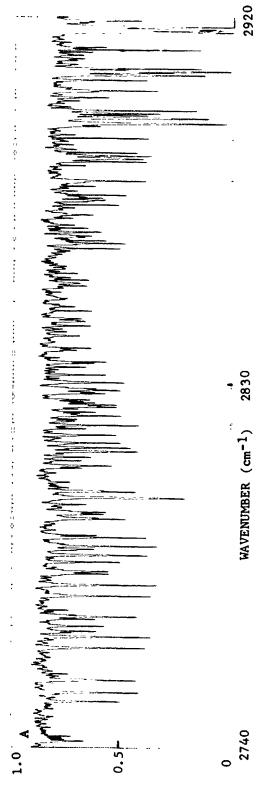




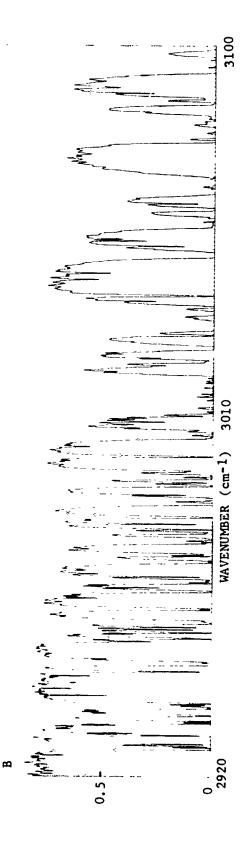
WAVENUMBER (cm^{-1})

0 ; l 2080

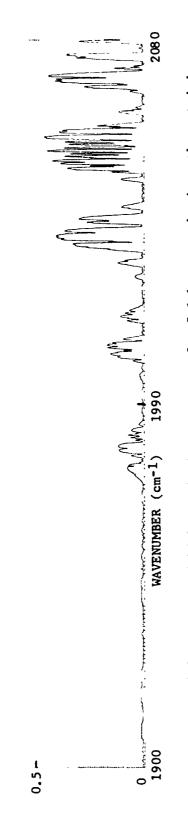




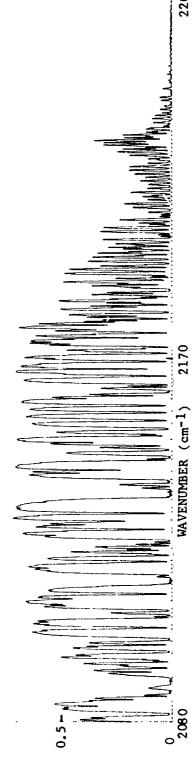
Measured high-resolution spectrum of a 5.1-km atmospheric path containing B: 2920 to 3100 cm⁻¹) (S042, A: 2740 to 2920 cm⁻¹, 2.5 Torr of H20 Figure 4.1c

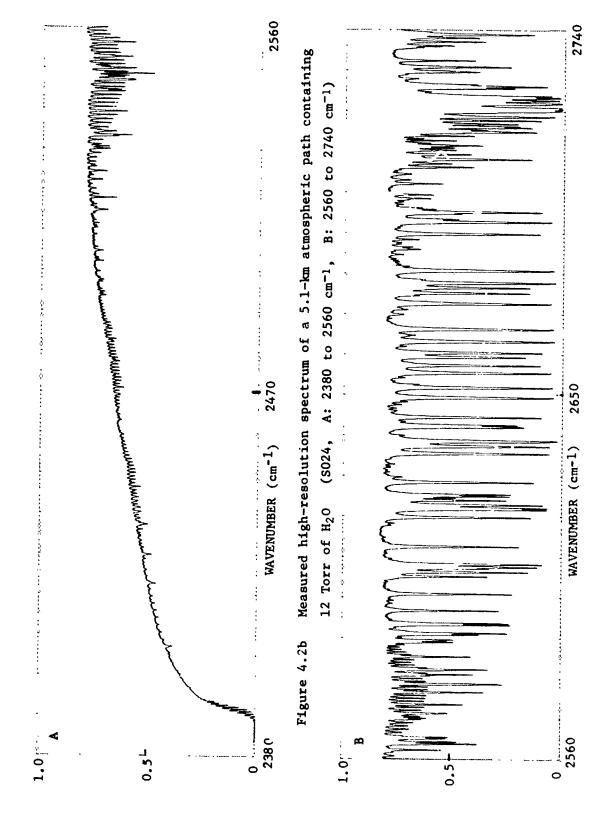


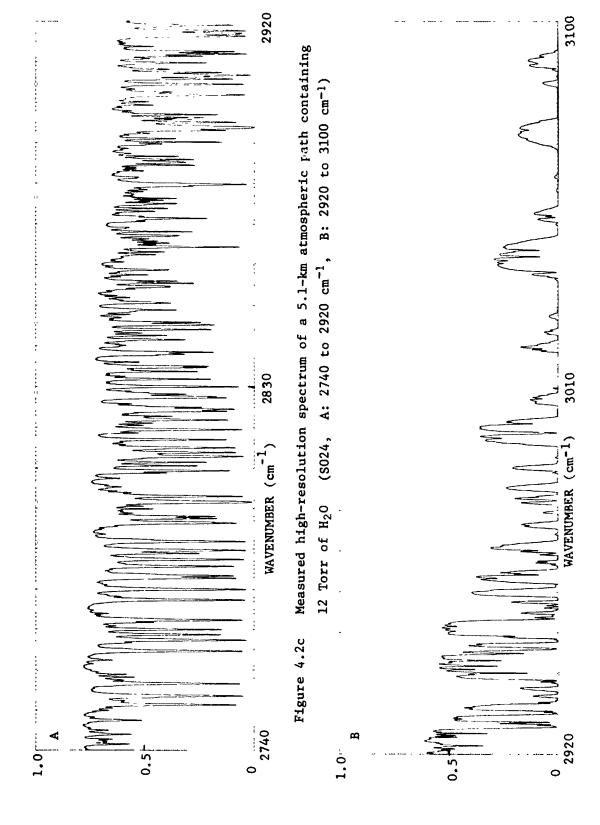


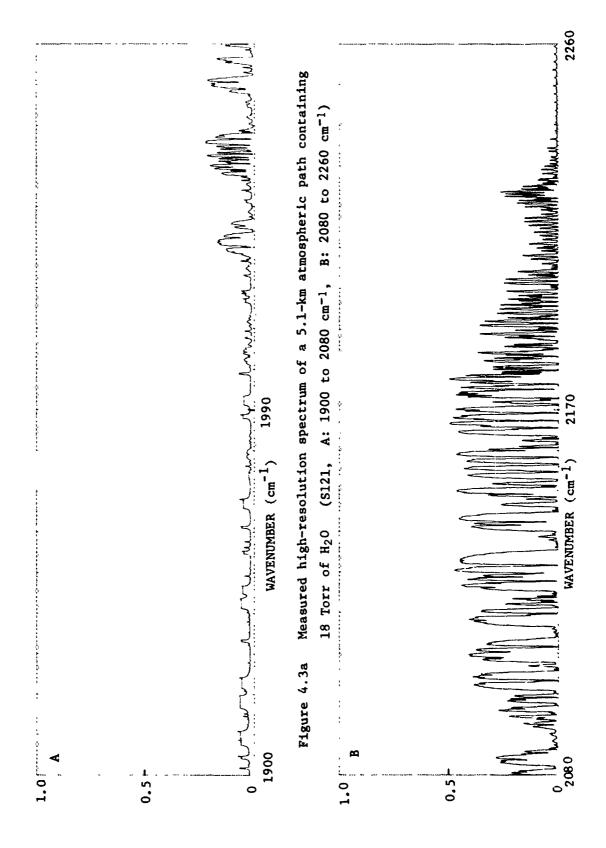


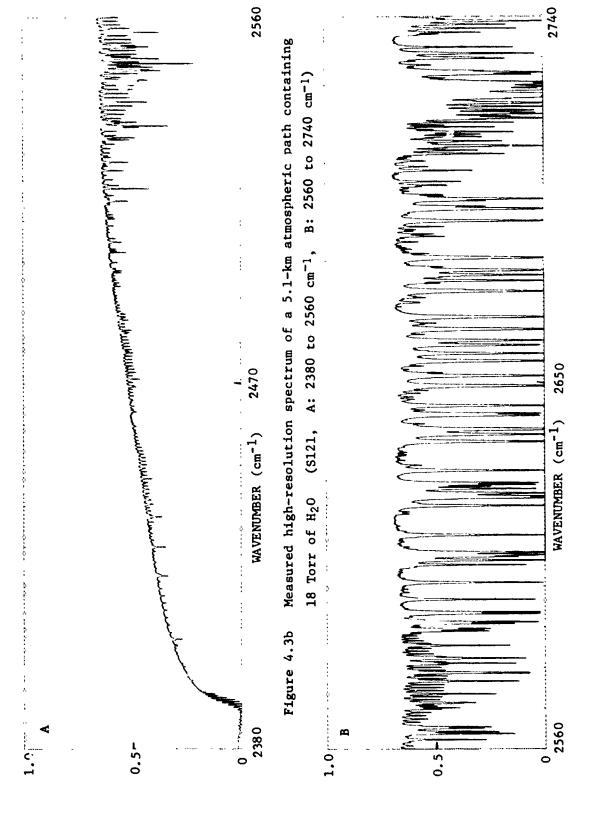












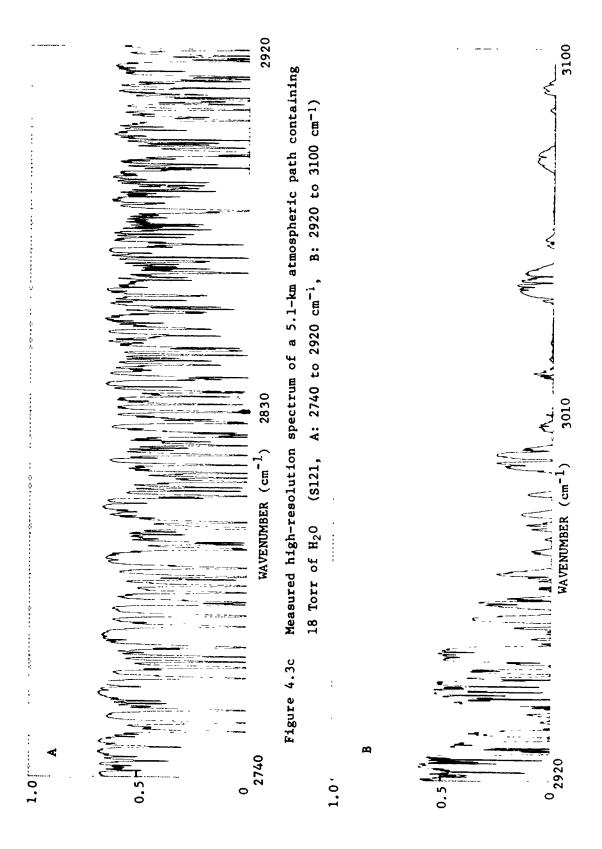
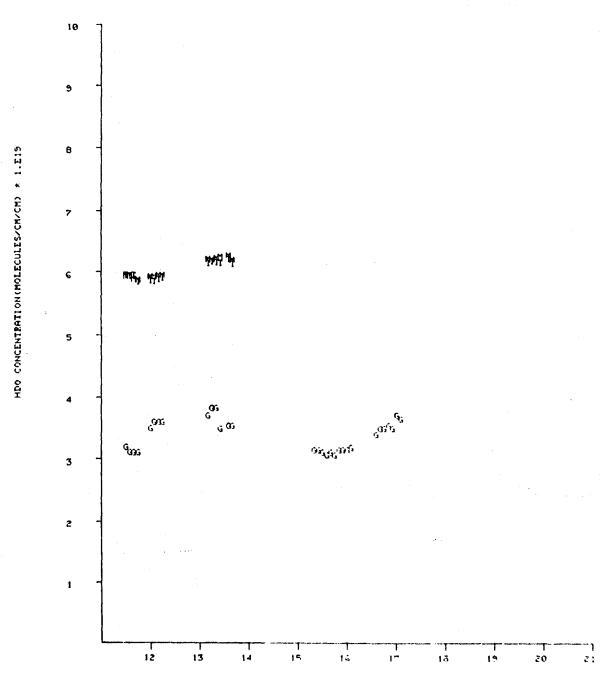


Fig. 5.1 INTEGRATED HDO CONCENTRATION (MOLECULES CHACH) FOR 5.12 km PATH, 3-MAR-77, CCAFS PATH TEMP. 15 DEG C. M-MOBILE MET STATION.T-TRANSMITTER MET.R-RECEIVER MET.G-GFGS



TIME 19 HOURS

Fig. 5.2 INTEGRATED HDO CONCENTRATION CHOLECULES CM CM) FOR 5.12 KM PATH. 4-MAR-77, CCAFS
PATH TEMP. 19 DEG C. M-MOBILE MET STATION, T-TRANSMITTER MET. R-RECEIVER MET. G-GFCS

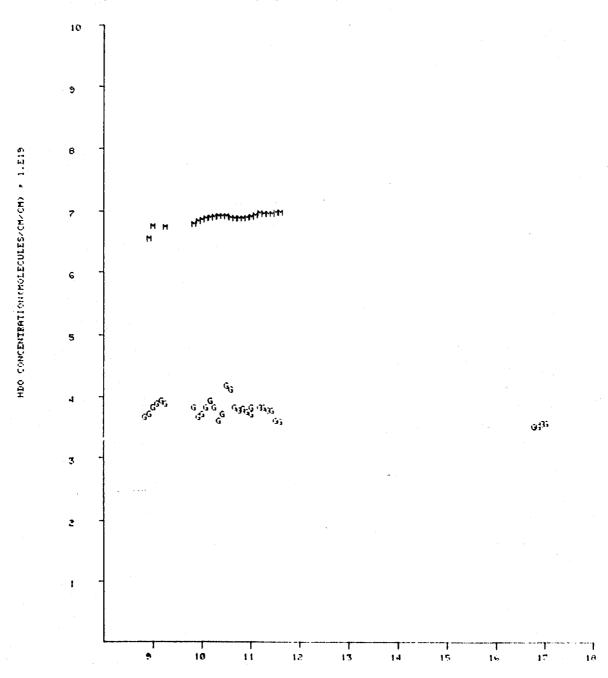


Fig. 5.3 INTEGRATED HDO CONCENTRATION (MOLECULES/CM/CM) FOR 5.12 KM PATH, "-MAR-77, CCAFS PATH TEMP. 24 DEG C. M-MOBILE MET STATION, T-TRANSMITTER MET, R-RECEIVER MET, G-GFCS

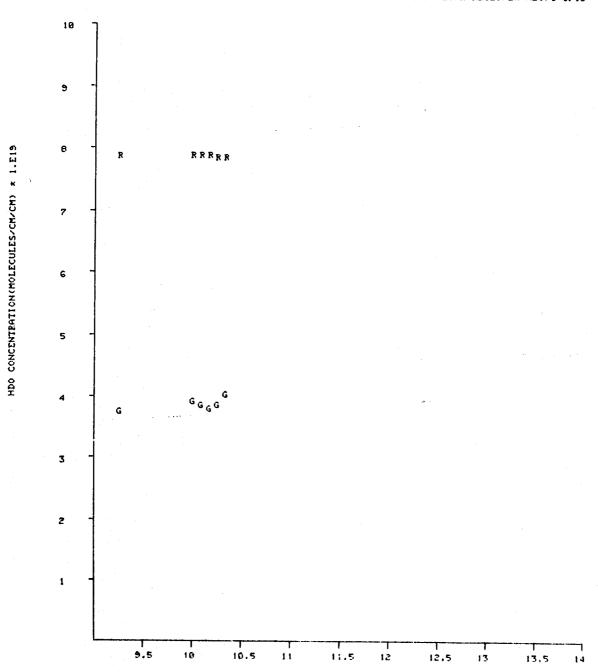


Fig. 5.4 INTEGRATED HOS CONCENTRATION MOLECULES ON CM. FOR 5.12 EM PATH. 8-MAR-77. CORES PATH TEMP. 21 DEG C. N-MOBILE MET STATION.T-TEMPSPITTER NET.R-RECEIVER MET.G-1FC:

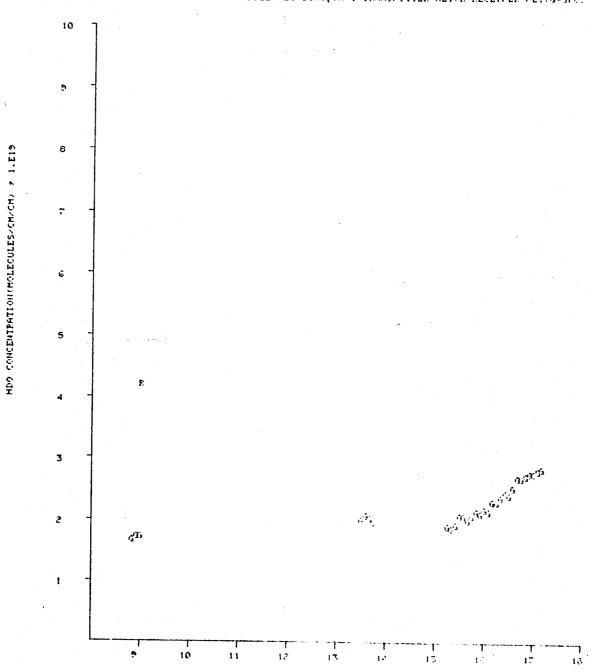


Fig. 5.5 INTEGRATED HDO CONCENTRATION (MOLECULES / CH. CH.) FOR 5.12 KM PATH. 9-MAR-77, CCHI > PATH TEMP. 19 DEG C. M-MOBILE MET STATION. T-TRANSMITTER MET. R-RECEIVER MET. G-GF13

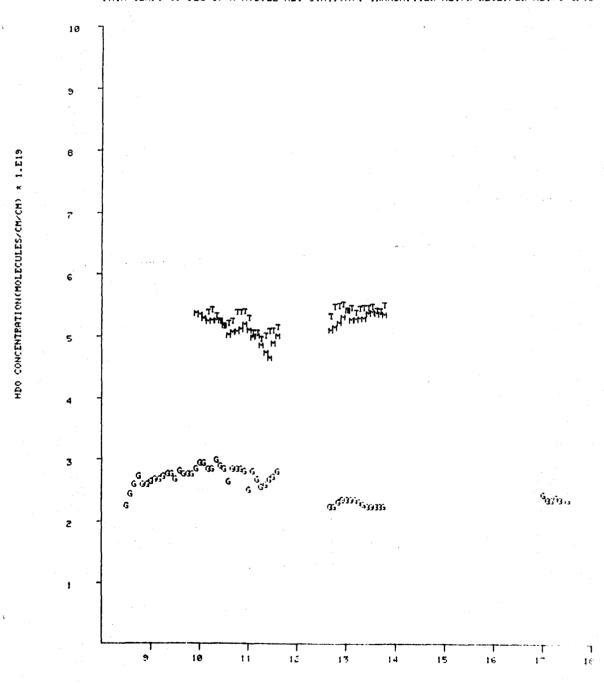
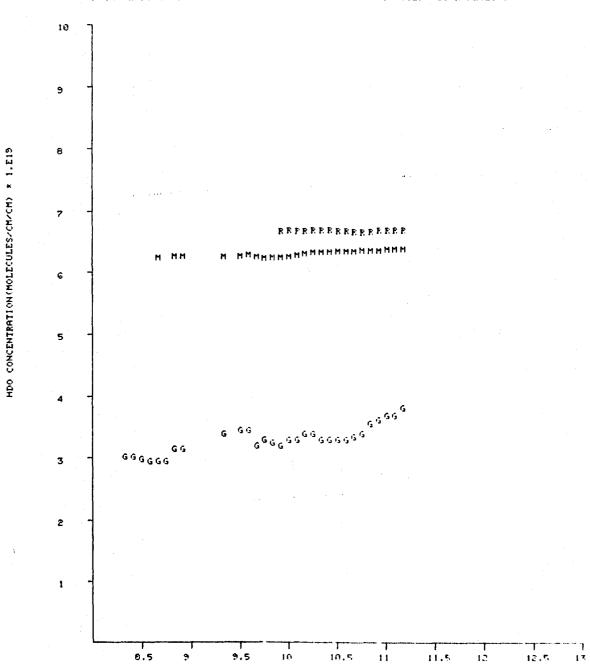


Fig. 5.6 Integrated add concentration(molecules/cm/cm) for 5.12 km path, 10-mar-77, ccafs
path temp. 18 deg c. M-mobile met station, t-transmitter met. R-receiver met. G-GFCS



TIME IN HOURS

Fig. 5.7 INTEGRATED HDG CONCENTRATION (MOLECULES ZCM ZCM) FOR 5.12 KM PATH, 11-MAR-77, CCAFS PATH TEMP. 19 DEG C. M-MOBILE MET STATION, T-TRANSMITTER MET, R-RECEIVER MET, G-GFCS

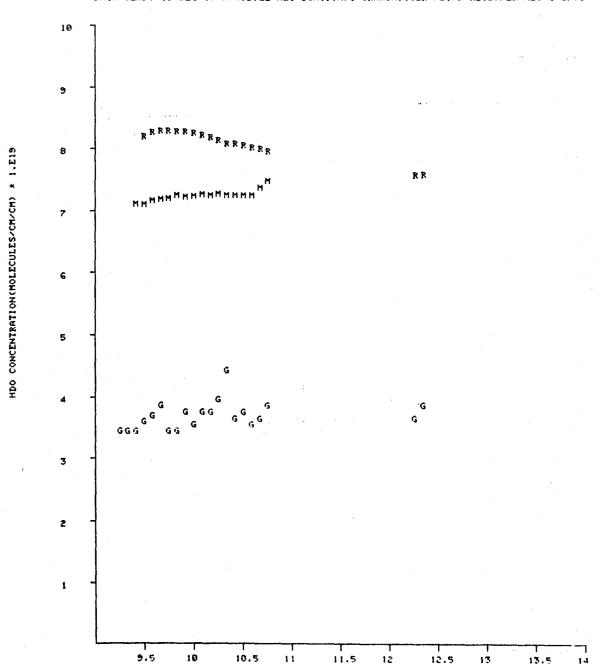


Fig. 5.8 INTEGRATED HDO CONCENTRATION (MOLECULES/CM/CM) FOR 5.12 KM PATH. 12-MAR-77, CCAFS PATH TEMP. 20 DEG C. M-MOBILE MET STATION, T-TRANSMITTER MET. R-RECEIVER MET. G-GFCS

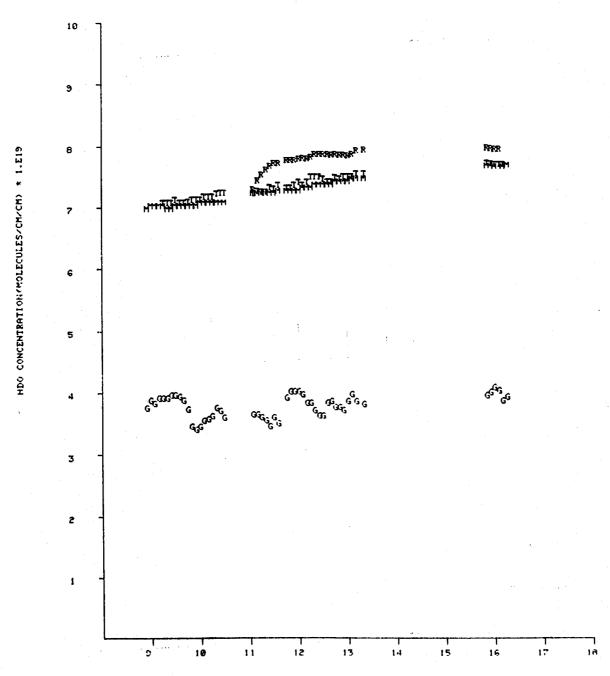


Fig. 5.9 INTEGRATED HDO CONCENTRATION (MOLECULES/CM/CM) FOR 5.12 KM PATH, 14-MAR-77, CCAFS PATH TEMP. 23 DEG C, M-MOBILE MET STATION, T-TRANSMITTER MET, R-RECEIVER MET, G-GFCE

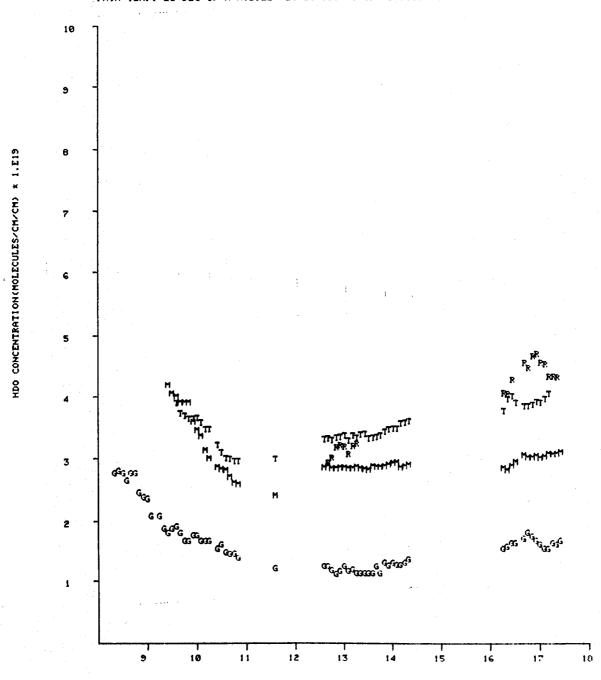


Fig. 5.10 INTEGRATED HDO CONCENTRATION (MOLECULES / CH/CM) FOR 5.12 km PATH, 15-MAR-77, CCAFS PATH TEMP. 28 DEG C. M-MOBILE MET STATION.T-TRANSMITTER MET.R-RECEIVER MET.G-GFCS

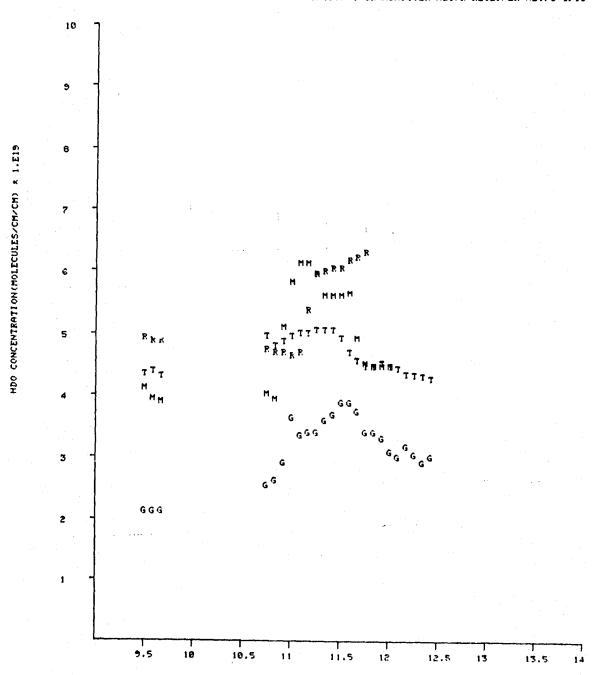


Fig. 5.11 INTEGRATED HDO CONCENTRATION (HOLECULES / CM / CM) FOR 5.12 KM PATH, 31-MAR-77. CCAFS PATH TEMP. 27 DEG C. M-MOBILE MET STATION.T-TRANSMITTER MET.R-RECEIVER MET.G-GFCS

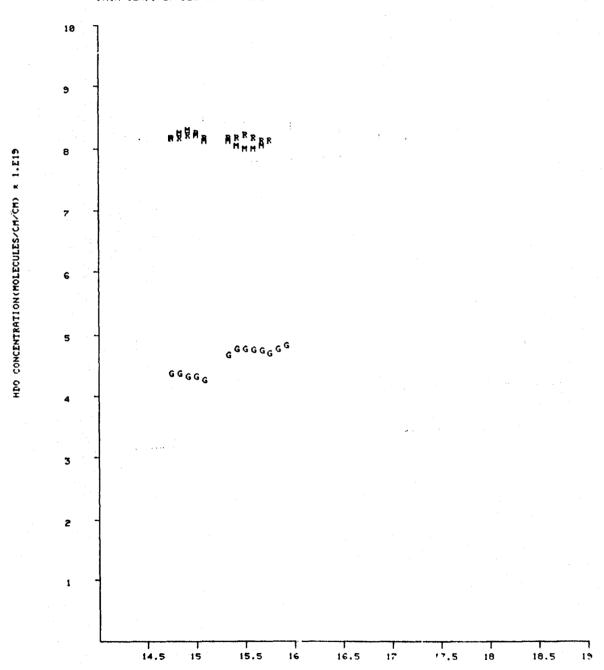


Fig. 5.12 INTEGRATED HDG CONCENTRATION (MOLECULES FOR 5.12 KM PATH, 1-APR-77, CCAFE PATH TEMP, 23 DEG C. M-MOBILE MET STATION, T-TRANSMITTER MET. R-RECEIVER MET. G-GFC:

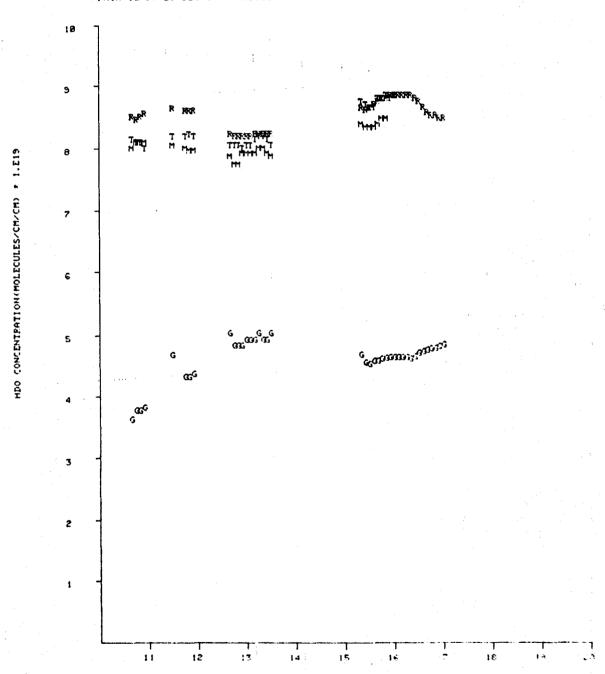


Fig. 5.13 INTEGRATED HDG CONCENTRATION (MOLECULES FCH. CH) FOR 5.12 KM PATH. 2-APE 27. CCAPT PATH TEMP. 24 DEG C. M-MOBILE MET STATION T TRANSMITTER MET. R-RECEIVER MET. 9-GPC

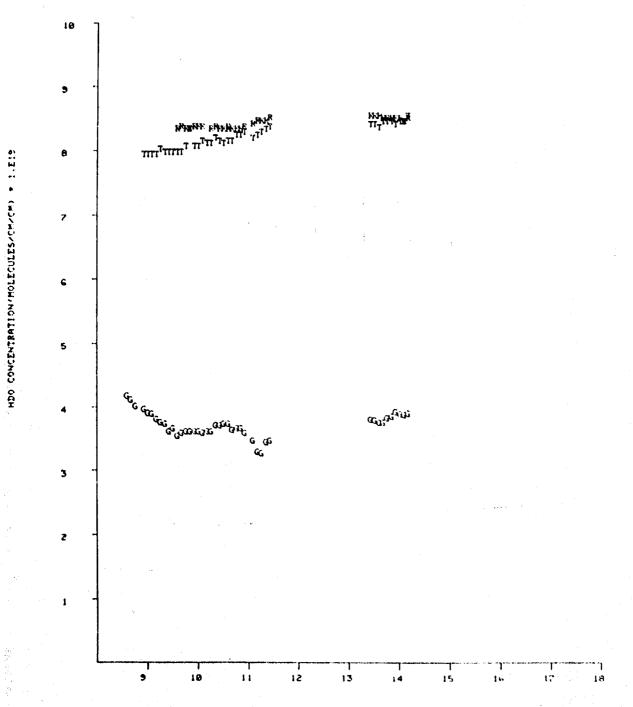
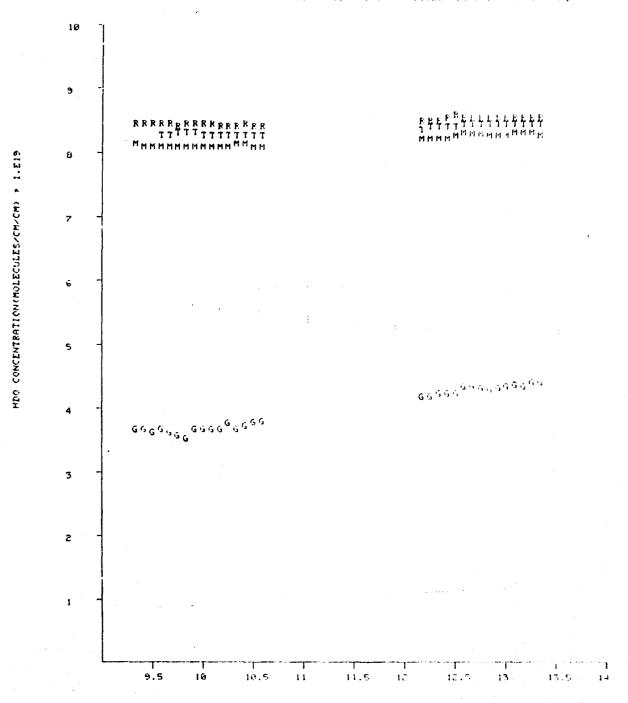


Fig. 5.14 INTEGRATED HDG CONCENTRATION CHOLEGULES CHICAGO FOR 5.12 ON TWIN 4-44 FOR CONF.

PATH TEMP. 24 DEG C. M-MOBILE MET STATION T-TRANSMITTER MET FOR SIVER MET, G-GFCS



一十二人是 医多种 医一种

Fig. 5.15 INTEGRATED HDG CONCENTRATION (MOLECULES (CM CM)) FOR 5.12 KM PHTH. 5-MEE-OV COMES PATH TEMP. 24 DEG C. M-MOBILE MET STATION T-TERMISMITTER MET. 8-RECEIVER MET. 6-0FOS

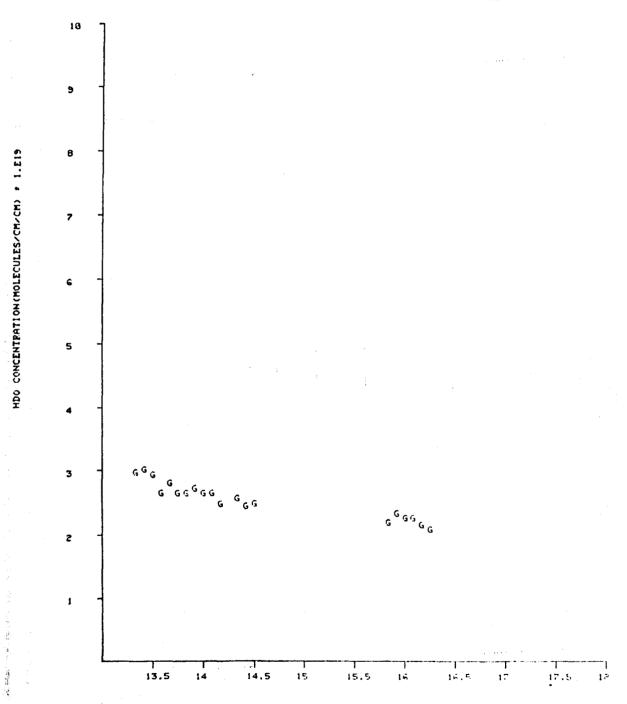


Fig. 5.16 INTEGRATED ADD CONCENTRATION MOLECULES CHOOKE FOR 5.12 KM CATH. 16-MAY-77. COARD PATH TEMP. 25 DEG C. M-MOBILE MET STATION TO PARISHITTER MET K-RECEIVER MET GOSFO.

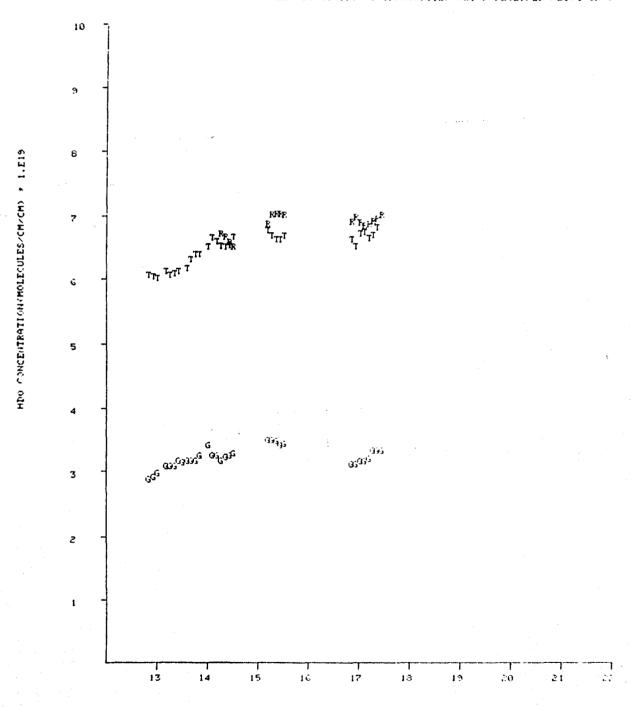


Fig. 5.17 INTEGRATED HDG CONCENTRATION MOLECULES (CM. CM) FOR 5.12 KM PATH, 17-MH)-77% CCHES PATH TEMP. 25 DEG C. M-MOBILE HET STATION T-TRANSMITTER HET.R-PECEIVEP HET G-GFCS

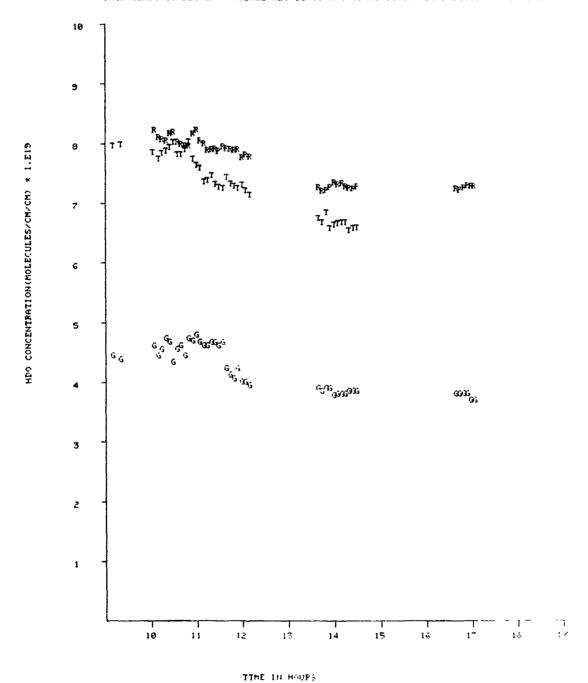


FIG. 5.18 INTOSENTED H. CONCENTENTION MOLE QUE. (M. M.) FOR \$1.12 OF ENTH (18-MH) -7 CONF.,
FIGH TEMP C. TEG C. M-MOBILE MET ETHION T-TENNIMITTEE MET F-FE/ENCEP MET 9-9F

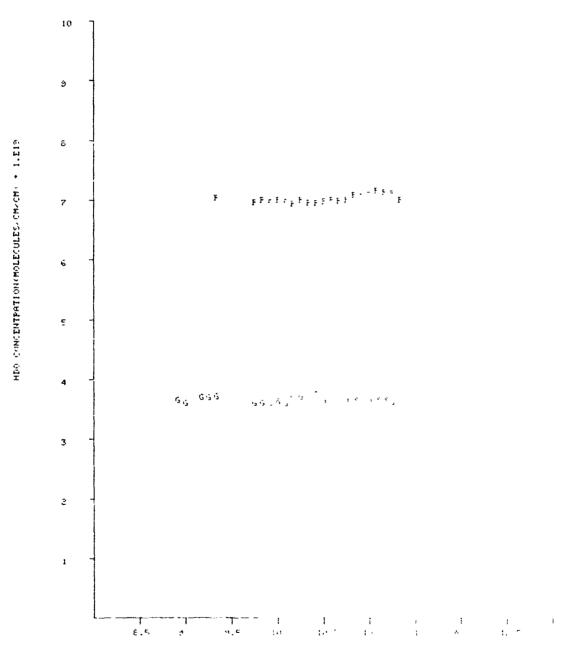


Fig. 5.19 INTEGRATED HDO CONCENTRATION/MOLECULES CM CM) FOR 5.12 km PATH, 20-MAY-77, CCHFS PATH TEMP. 28 DEG C. M-MOBILE HET STATION.T-TPANSMITTER HET.R-RECEIVER MET.G-SFCE

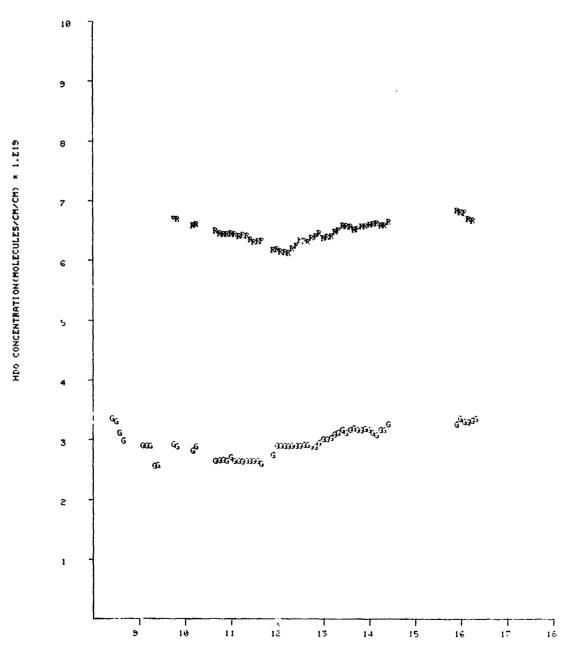


Fig. 5.20 INTEGRATED HDG CONCENTRATION MOLECULES ON ONE FOR SUB-RM ENTH. CI-MAY-TT. COMPS PATH TEMPS DG DEG C. M-MOBILE MET STHILON T-TEMPSMITTER MET F RECEIVER MET G-GFGCS

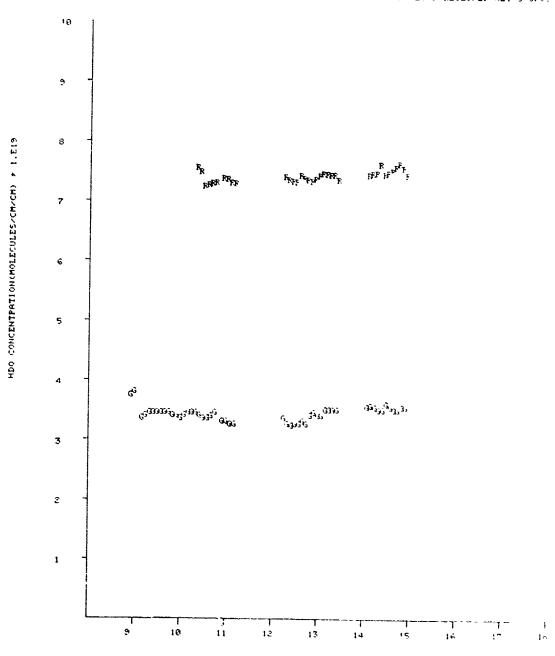


Fig. 5.21 INTEGRATED HDG CONCENTRATION (HOLECULES CM CM) FOR 5.12 (M PATH 23-MAY-TT CCAF PATH TEMPS 26 DEG C M-MOBILE MET 1.ATION T-TEHNEMITTER MET F-RECEIVER MET G-GECT

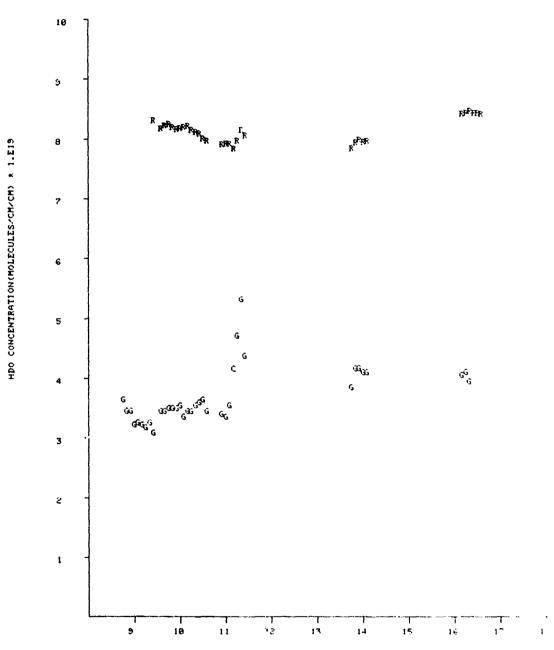


Fig. 5.22 INTEGENTED OFF CONCENTENTION MOLECULE. ON THE FOR FIRE FATHER 24-MAY-TT CONTENT PATH TEME, 28 DEG C. M-MOBILE MET STATION THIRM MITTER MET E-PECEICEP MET G-6FG.

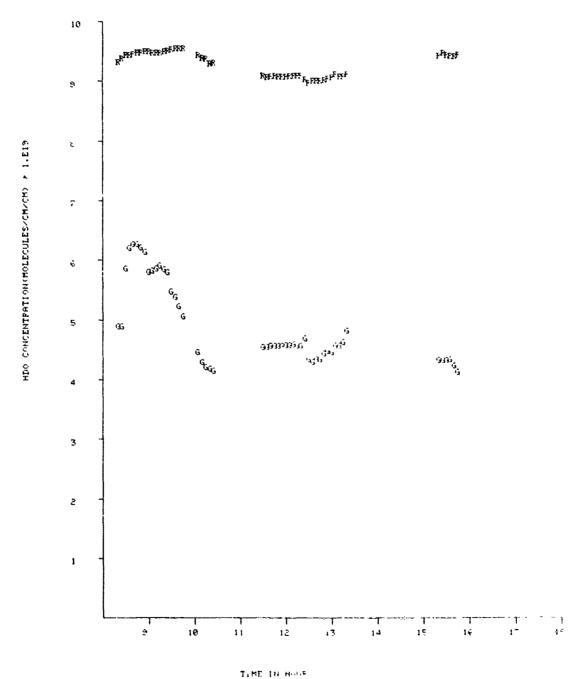
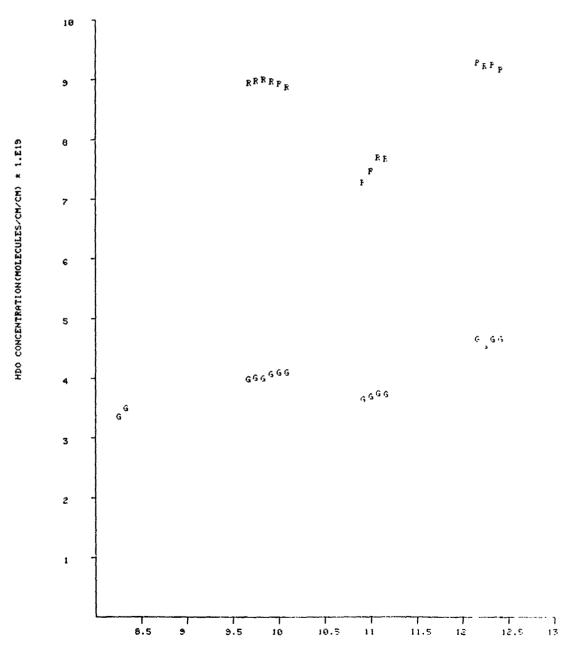


Fig. 5.23 INTEGRATED HDG CONCENTRATION/HOLECULES/CH (H) FOR 5.12 (M PHTH, 25-MHY-7, CCHFS PATH TEMF, 30 DEG C M-MOBILE MET STHTIUN/T-TRHUSHITTEP MET/E-PECEIDEF MET/G-GFCS



TIME IN HOUPE

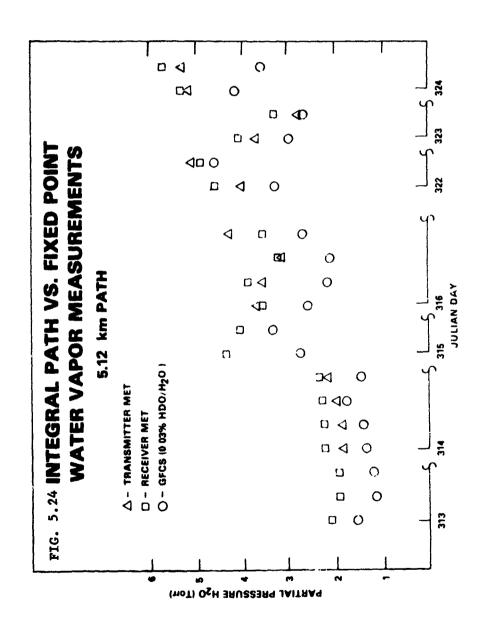


Table 6.1.1. Bagic meteorological data for the period 23 February through 25 May 1977 as measured at the Cape Canaveral laser test site (see Section 6.1 for definitions).

ı	WOH (DEG)								~	=	0	4	3	\sim	4	Ľ,	9	9	∞	œ	209	~	~	2	δ	-	Φ			
	HS (M/S)	•	•	•	•	•	8.2	•	•	•	•	•	•	•	•		•	•	•	•	•		•	•	•	•	•		•	•
,	SR CW/SO M)	44	3	63		.3	0.37	.3	.	.3	.3	.3	3	3	.3	•	6.	8	•	5	€,	.2	0.	6.	0	0	1	-		0
	BP (MBAR)	018.	017.	017.	017.	016.	1016.8	016.	019.	019.	019.	019.	018.	018.	018.	017.	017.	017.	017.	017.	017.	017.	017.	017.	017.	017.	017.	017.	016.	016.
	#	4	-	+	5	-	87.6	-	0	•	4.	6	6	-	2	5	-	-	•	2.	1.	4	3.	.	œ	3	6	œ	6	œ
i	PPH2G (TORR)	3.2	3.4	3.5	3.4	3.2	13.15	3.1	9.3	0.0	0.2	0.3	0.3	0.5	0.3	1.3	1.6	1.8	2.3	2.5	• 6	2.8	2.6	4.1	4.1	4.7	4.6	4.9	4 • 8	5.1
	AT (DEG)	œ	6	æ	8	P.	17.5	7	8	•	•	7.		-	-	-	7	-	-1		7.		7	*	œ	0	8	•	6	9
:	SITE	-	-	-	j- -	-	-	-	-	_	-	-	-	-	-	_	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	TIME	4.3	50	53	9	63	1700	73	10	13	20	23	30	33	40	43	50	53	60	3	70	73	80	03	10	13	20	67	30	33
	YFAR	7.7	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11
	IFRE	Ū.	ū	ī	ш	Ĭ.	FE8	ŭ,	ŭ	ū	w	W	ų,	ш	ш	ш	ij.	u	ũ	ii.	ш	ш	ù.	w	ш	ш	ш	ũ.	ù	LL.
	DAY						23																							

Lable 6.1.1 (continued)

UAY	I NO	YEAR	7 I ME	SITE	AT (DEG)	PPH2G (TORR)	8 H	BP (MBAR)	SR (W/SQ M)	WS (M/S)	WOH (DEG)
		7.7	40	-	•	4.9	5	016.	0	•	-
		11	43		6	4.9	5.	015.	6.	•	_
		11	50	 -	6	5.1	-	015.	8	•	-
		11	53	j-	6	5.3	8	015.	-	•	-
		11	9	j	9	4.	•	015.	• 6	•	-
		11	6.3	-	6	5.5	-	015.	4.		
		11	70	-	9.	5.5	2.	015.	• 2	•	-
		11	23	-	e.	6.	9	018.	• 5	•	-
87		11	23	١-	*		9	018.	4	•	5
		11	30	-	3		2	017.	.2	•	∞
		11	33	;- -	3	0	2	016.	.2	•	∞
		11	0,7	3 .	4	6.	6	020.	•2	•	4
		11	40	-	4	0	8	016.	Š	•	•
		*-	5	Z	4.	0.	·:	020	•2	•	~
		11	43	- -	3.		80	016.	•2	•	9
		11	50	-	3	\sim	~	016.	6	•	8
		11	53	-	4	3	•	016.	•2	•	\sim
		17	9	-	4	2.	•	016.	.3		~
		11	63	-	*	.3		016.	.2	•	-
		11	20	_	4.	•	3.	017.	•	•	4
		7.7	73	-	3	6.	6	017.	0	•	\vdash
		11	80	-	.	• 2	-	017.	•	•	5
~		11	10	E	8	• 6	5	027.	•	•	S
-		11	10	- -	5	8		022.	0	•	4
~*		11	13	S.	\$	~	-	027.	-	•	~
~		11	20	x	٥.	• 5	2	027.	-	•	~
, -	N A E	11	1230	¥	15.5	4.42	33.6	1027.2	1.21		261
~		11	30	-	4.	4.	<u>.</u>	021.	7	•	0
7		11	33	† -	÷		•	021.	7	5.8	4

Table 6.1.1 (continued)

UAY	HONDH	YEAR	TIME	STTE	A	pH2				K	HOM
					(DEG)	(TORR)	(2)	(MBAR)	CH OS/H)	(H/S)	(DEG)
~	⋖		40	-	4	2	3	021.			0
-	⋖		4 3	-	4	4.	5.	021.	0	•	207
7	⋖		50	-	4		-	020.	6	•	-
,1	•		~	-	3	æ	æ	020.	8	•	œ
~	⋖		60	-	4.	.2	6	020.	•	•	75
~	ď		63	_	4	*	5	920.	•5	•	51
2	Q.		0	¥	<u>ئ</u>	•	1:	027.	3	•	2
7	HAR	77	930	 - -	15.8	5.49	40.9	1023.4	0.73	2.8	270
~	⋖		93	Æ	•	•2		027.	. 7	•	~
7	⋖		00	-	\$	o.	5.	023.	φ.	•	9
7	⋖		00	æ	\$		-	028.	8	•	5
7	⋖		03	-	9	• 6	2	923.	6.	•	117
7	◂		03	¥	œ.	~	4.	028.	6.	•	4
7	⋖		10	-	7	• 2	5	023.	0		8.7
7	⋖		10	Œ	æ	4.	•	\$500	•	•	31
~	⋖		13	-	•	œ	3,	£23.	•	•	131
7	⋖		13	Z	œ	*	*	028.	7	•	~
7	⋖		0	-	•	.5	. • ₹2	023.	7		70
7	⋖		20	-	.0	6.	7	024·	6.	•	54
2	⋖		23	L .	پ	9	7.	023.	1.		79
~	⋖		53	Ŧ				028.	7.		23
~	•		3	•	•	α.	&	022.	0	•	173
7	ব		30	Æ	-	0	0	028.	6.	•	(
7	₹.		33	-	•	9.	3.	022.	7		36
7	⋖		33	*	8		3.	027.			35
7	◂		0	-	17.0	7.92	54.8	022.	0	•	66
~	•4		40	æ	-	.3	8	027.	0	•	40
7	⋖		43	-	•	6.	•	022.	6.		4.3
~	⋖		43	X	7	.5	6	027.	0		58

Table 6.1.1 (continued)

UAY	E E	YEAR	TIME	SITE	AT (DEG)	PPH2G (TGRR)	# *	8P (#8AR)	SR (H/SQ H)	HS (H/S)	WDH (DEG)
~	•		50	Æ				027.	6	•	
7	HAR	11	1530	I	~	6	>	1026.4	0.79	0.7	32
(C)	⋖		8	-	7	1.6	-	020	4	•	
m	◀		00	*	17.5	11.73	78.4	025.	9	•	0
m	◀		03	-	-	1.8	-	020	œ	•	
M	◂		03	x	4	9.0	;	025.	~	•	-
m	•		10	-	-	7.4	?	021.	9	•	0
m	⋖		10	×	-	2.3	2	025.	.5	•	N
~	⋖		13	-	œ	2.7	-	020	œ	•	Œ
m	⋖		13	×	-	2.7		025.	~		0
m	⋖		20	-	œ	2.5	-	020.	~	•	6
m	◂		20	*	-	2.6	3.	024.	٥	•	0
m	Œ		23	-	7	2.7	3.	020	0	•	O
m	4		23	X .	1.	1	3.	024.	• 6	•	-
~	⋖		30	- -	7	3.1	5	019.	0	•	
M	•		30	æ	-	3.1	•	023.	4.	•	-
m	•		33)-	6	3.3		019.	4		0
C	4		33	•	œ	3.4	3.	023.	7.	•	
m	•		6	-	œ.	3.2	?	019.	0	•	σ
E	⋖		43	-	œ	3.4	•	018.	6	•	0
e.	⋖		20	-	8	3.2	•	018.	8	•	ø
*	•		Ō	æ	œ	4.6	4	019.	5	•	•
•	•		~	×	&	4.6	3	019.	~	•	•
4	•		8	#	œ	4.8	2	019.	ω,	•	50
•	⋖		10	*	œ	4.9		020.	0	•	80
4	◀		13	=	6	5.1	•	020	•	•	5
•	⋖		0	x	6	5.2	•	020	8	ě	
•	•		23	#	•	5.4	~	020	S	•	4
4	◂		30	٦.	6	5.5	-	020	0	•	4

Table 6.1.1 (continued)

-	HONDE	YEAR	TIME	SITE	AT	PPH20	¥	œ			HOM
					(DE6)	(TORR)	£	(MBAR)	CH DS/H)	(M/S)	(050)
•		11	3	æ	6	5		019	-	•	. V
*		77	9	E	6	7		019	9	•	ľ
4	MAR	11	1430	X	19.8	15.59	90.3	1019.4	96-0	-3	151
4		11	50	X	ċ	5.6		018	0	•	· L
4		11	53	æ	6	5.7		018	~	•	S
<u></u>		77	900	S	2	7.2		017	4)	•
-		11	930	S	6	7.3		018	-		, 0
_		11	8	S	4	6.7		018	-		, , ,
~		11	6	S	3	7.3		018			٠. ١
~		11	10	v.	•	7.2		018	7		4
_		11	=	S		5.9		018	7		•
~		11	20	S	7	6.6		017	-		٠ ٧
~		11	23	S	8	6.6		017	,		(
~		77	1300	S	œ	5.3		017	4		~
~		11	33	S	6	3.2		017	-		-
~		11	9	S	æ	3.0		017	-		71
~		11	43	S	-	2.5		017	-		4
_		11	50	S	9	2.2		019	7		α Φ
~		11	53	S	•	1.9		018			9 6
~		11	8	S	5	1.7		018	7		23
~		11	63	S	5	1.8	•	018			23
~		11	20	S	5	1.7		019	7		21
œ		11	006	S	8	1.1			1		i
œ		11	930	S	0	8					
ဆ		22	8	-	6	6	•	021.	0	•	
5		11	9	=		9		1028.1	0.25	0.5	7.0
20		11	00	S	•	9.5)) 	;	•	
S		11	1030	_	œ	~		024.	2		09
σ		11	03	æ	-	1.2		1028.4	0.63	1.0	~ ~
								1)		

Table 6.1.1 (continued)

DAY	I P Z D E	VFAR	TIME	SITE	AT (DEG)	PPH2G (TGRR)	RH (2)	RP (MBAR)	SR (W/SQ M)	WS (M/S)	WDH CDEG)
30	⋖	11	60	S	•		-				
6	4	11	10	_	80	1.5	2	024.	~	•	49
J	⋖	11	10	ĸ	7	1.0	3	028.	9.		7.8
σ	•	11	13	_	9.	1.0	\$	023.	5		55
6	•	11	13	E	9	0.5	4	028.		•	69
σ	•	11	20	-	• 6	1.1	4	023.	φ,	•	57
Ś	MAR	11	1200	æ	18.7	10.68	6.	028.	• 2		11
ው	•	11	23	_	•	1.0	2.	023.	• 2		55
5	⋖	11	23	æ	6	0.5	3.	027.	.2	•	76
2	◂	11	30	_	•	1.7	5.	022.	7	•	63
တ	₫	11	30	X	œ	1.4	0	027.	7		7.5
6	•	11	33	-	9.	1.9	-	022.	0.	•	19
σ	◂	11	33	X	8	1.6	•	027.	7	•	81
5	41	11	6	-	е С	1.9	4	022.	0		7.2
6	•	11	*	-	9.	1.9	•	021.	6.		99
ઝ	•	11	50	-	0	1.1	3.	021.	. 7		5.7
σ	40	11	53	-	6	1.4	~	021.	9,	•	8 9
5	•	11	9	-	9.	0.9	*	021.	4.		63
	•	11	15	S	8	2.2	5.	024.	7		59
10	•	11	90	X	-	3.5	•	021.	•2	•	40
	•	11	93	E .	7.	3.5	8	021.	9.		96
	•	11	00	Æ	8	3.5	-	021.	ij.	•	•
	•	11	00	v	.	4.4	&	020.	.3		-
	-	11	03	×	æ	3.6	7.	022.	2		0
	•	11	03	S	6	4.4	•	020.	~	•	0
	45	11	10	*	*	3.7	å	021.	.2		~
	-	11		S	•	4.4	7.	020	4.	•	112
	•	11	13	X	7.	3.7	6	021.	5	•	-
	•	11	13	V	9.	4.6	84.8	1020.8	99.0	2.3	-4

Table 6.1.1 (continued)

DAY	HINDH	YFAR	TIME	SITE		PPH26	Ξ	9	SR	SE	HOM
					(DEG)	T OR					Ū
	⋖	11	20	æ	*	3.7	80	021.	.5	•	0
	◂		20	S	6	4.7	*	020.	9	•	-
	⋖		23	X	æ	3.7	8	021.	m	•	Ö
	⋖		23	S	6	4.6	5.	020.	4		104
10	MAR	11		S	0			020.	9		69
	⋖		33	S	•	4.3		019.	4.	•	82
	Œ		40	-	8	4.4	8	016.	7	•	65
	◂		6	S	6	4.2	2.	019.	3	•	0
	⋖		4 3	-	6	4.6	3	016.	-	•	61
	⋖		43	S	0	4.3	2.	019.	£.	•	62
	⋖		50	S	•	4.6	1.	019.	۳.	•	64
	⋖		53	S	•	5.0	2	019.	.3	•	58
	⋖		93	E .	8	5.4	•	021.	£.	•	S
	⋖		00	Æ	•	5.6	5.	021.	3	•	112
	⋖		03	Œ	6	5.7	\$	021.	3	•	æ
	⋖		10	Æ	6	6.0	•	022.	0	•	_
	⋖		13	S	?	5.8	.	020.	-	•	
	⋖		20	S	2.	6.2	-	020.	9	•	0
	⋖		23	S	-	6.4	*	020	0	•	0
	⋖		0	S	2.	6.5	8	020		•	16
	⋖		33	S	2.	6.7	•	.610	۲.	•	86
	⋖		40	S	2	9.9	•	019.	6	•	0
	⋖		43	S	2	6.8	÷	019.	6.	•	-
	⋖		20	S		6.9	6	019.	6.	•	101
	⋖		53	S	3.	6.8	&	018.	9		σ
	⋖		9	S	3	6.B	-	019.	• 6	•	18
	⋖		63	S	2.	9.9	•	018.	• 5	•	0
	⋖		90	ĸ	6	5.5	2.	021.	5	•	120
	⋖	11	930	-	19.3	4		1017.7	0.61	2.8	0

Table 5.1,1 (continued)

THE PROPERTY OF THE PROPERTY O

E A A	I N	YEAR	TIME	SITE	AT (DEG)	PPH2G (TORR)	# £	BP (MBAR)	SR (W/SQ/M)	WS (M/S)	WDH (DEG)
12	•	11	(1)	2	6	5.2	1.	021.	\$	•	~
12	H R	11	1000	-	19.4	15.53	91.9	1017.8	0.71	5.6	115
	⋖	11	00	Æ	6	5.3	-	021.		•	~
	◂		03	-	9.	5.7		017.	φ,	•	-
	₫		\mathbf{c}	=	•	5.4	-	021.	φ,	•	4
	⋖		10	#	6	5.6	0	021.	0	•	4
	⋖		7	S	3	6.6	• 9	020.	•		4
	⋖		ä	-	6	5.8	•	017.	0	•	~
	•		13	×	0	5.7	•	021.	0	4.0	4
	⋖		15	S	4	6.9	5.	020	***		4
	Ø		20	-	•	6.1	•	016.	0	•	-
	⋖		20	×	•	5.8	6	021.	0	4.0	چ.
	⋖		22	S	+	7.0	*	019.	~		Ť
	⋖		23	-	•	6.1	6	017.	٦,	•	-
	⋖		23	•	ċ	5.9	œ	020.	6.	4.0	5
	⋖		25	S		7.0	Š	019.	•		•
	•		30	>	•	¢.3	-	016.	7		m
	⋖		30	×	ċ	6.1	œ	020.	7.	0.3	4
	⋖		32	'n	*	7.2	5	019.	•		4
	•	11	33	-	•	4.9	-	016.	0	•	\sim
	•		33	氰	ċ	6.2	å	020.	8	0.3	3
	⋖		35	S	3.	7.0	-	018.	7	•	3
	⋖		9	-	•	6.5	2.	015.	•	•	~
	⋖		40	Œ	ö	6.4	ö	019.	•		3
	⋖		42	S	•	7.3	\$	017.	0		4
	⋖		43	-	0	6.8	~	015.	0		\mathbf{c}
	◀		43	*	;	6.6		019.	0	9.0	4
	⋖		45	S	•	7.3	3.	017.	Ş		4
	⋖		50	}	•	6.7	w.	015.	• 9	3.1	33

Table 6.1.1 (continued)

UAY	ICACE	YEAR	TIME	SITE	AT	PH2	I	8	œ	X.	HOR
				1	(DEG)	(TORR)	3	(MRAR)	CH/SO H)	(8/H)	(DEG)
	⋖	11	50	Æ	0	6.7	•	18	6.	7.0	151
	⋖	11	52	رم د	4	7.3	5	017.	æ		4
	⋖	11	53	x	0	9.9	-	013.	œ	9.0	.1
	⋖	LL	55	S	3	.2	6	017.	۲.		((1)
	⋖	11	9	Œ	0	9.9	2.	018.	-	•	3
	⋖	11	63	æ	ő	6.6	1.	018.	5	•	~
	⋖	11	70	×	0	6.6	2	018.	4.	•	C
	⋖	11	93	Æ	2.	8.9	2	019.	~	•	C
	⋖	11	00	-	3	0	80	015.	6.		~
	⋖	11	00	¥	3	3	5	019.	\$		
	⋖	11	92	S	•	•	-	018.	0.		
	⋖	11	03	-	3.	α·	-	015.	0	•	
	⋖	11	03	x	۳.	2	8	019.	6.	•	
14	MAK	11	1100	-	23.6	99.9	30.4	015.	1.10	2.8	8 2
	⋖	11	10	Æ	4	\$	*	019.	0	2	
	⋖	77	=3	-	щ.	5.	6	015.	1.	•	
	⋖	11	13	×	\$		3,	019.	-1	•	
	•	11	20	~	3.	Š	0	015.	? •		
	⋖	11	20	#	*	4.	3.	019.	7.	•	
	⋖	11	23	-	3.	~	2.	015.	4	•	
	•	11	23	X	4.	•	•	019.	• 2	•	
	4	11	25	s	\$	0	~	017.	• 2		
	⋖	Li	30	-	3.	.	•	015.	•2	•	
	⋖	11	30	æ	4.	٠,	-	018.	٠,	1.0	
	⋖	11	33	-	۶.	2	3.	014.	2.	•	
	Ø	11	33	3	4	7	•	018.	٦.	•	
	⋖	11	60	-	3.	٠,	5	014.	~	•	
	⋖	11	9	Æ	*	•	-	018.	7		
	•	22	43	-	6	7	-	014.	0	•	

[able 6.1.1 (continued)

UAY	エースでは	YEAR	TIME	SITE	AT	DZHdd	I X	80	æs	SE	HOM
					(DEG)	10A	£	(MRAR)		(M/S)	(010)
	4		4.3	¥	*	4	œ	017.	0	0.9	
	⋖		45	S	•	6	9	016.	-		
	4		50	-	2	2.	•	014.	6.		
7 4	a a a	11	1500	×	24.2	6.18	~	17	6.	0.8	26
	⋖		53	-	2	-	•	014.	φ,	•	
	Æ		53	×	3.	0	-	017.	80		
	⋖		55	'n	4		6	016.	~		
	<4		9	ىحو	2.	0	5	013.	-	•	
	⋖		9	*	<i>ن</i> •	• 2	6	017.	9	6.0	
	⋖		6 2	S	3,		2	016.	5		
	⋖		63	_	2	5	~	013.	9	•	
	⋖		63	×	3.	4.	•	016.	• 5	0.9	
	⋖		65	S	3.	.2	œ	016.	*		
	⋖		20	_	:	• 5	3.	013.	4	•	
	⋖		2	×	2.	.5	2.	016.	4.	0.8	
	Ø		73	¥	-		4	.910	?•	•	
	Ø		5	S	پ	6.	5.	018.	.		C,
	⋖		0	×	-	4.6	•	019.	9		0
	⋖		2	S	4.	6.	•	018.	•	٦	-
	q		3	-	2.	• 6	•	015.	æ	•	0
	⋖		3	æ	2.	9.1	•	019.	8	•	0
	⋖		5	S	5.	6.	6	018.	φ,	•	œ
	€3		င္မ	-	٠ ش	8.9	-	015.	6.		\sim
	⋖		00	×	3.	• 5	8	019.	6.	•	δ
	⋖		02	S	~	9.0	6	018.	0	•	~
	⋖		03	 -	-	1.8	•	015.	•	•	3
	4		3	ĸ	*	6.	6	019.	•	•	
	⋖		05	د	œ	0.3	•	018.	~	•	
	•		10	-	3.	1.0	•	015.	1.14	2.8	5.0

Table 6.1.1 (continued)

CAY	HONIH	YEAR	TIME	SITE	AT (DEG)	PPH2G (TBRR)	# 3	BP (MBAR)	SR (W/SQ R)	WS (M/S)	WOH CDEG)
	⋖		-	Æ	•	2.9		016.	•	•	2
	Q		12	S	?	3.5	•	019.	.2	•	
	⋖		13	 - -	3.	1.0	2.	015.	.2	•	~
15	MAR	11	1130	x	21.7	12.51	64.3	1019.5	1.18	8.0	128
	⋖		20	-	£,	0.0	•	015.	•2	•	-
	⋖		20	X	•	0.0	6	019.	.2	•	
	⋖		23	-	4	9.4	-	015.	.2	•	
	⋖		30	-	8	-	6	015.	•2		
	•		33	-	3.	•	5	014.	7		
	4		43	-	3,	. 7	•	014.	0	•	
	€,		50	-	Š	œ	•	014.	6.	•	
	⋖		00	-		6.5	-	015.	6.	•	
	◁		03	-	<u>ج</u>	6.8	•	015.	0	•	∞
	₫		10	-	*	6.9	2	015.	۴-	•	3
	⋖		13	-	۲,	6.7	œ	014.	, 2	•	~
	⋖		20	-	Ϊ.	7.1	-	014.	6.	•	
	⋖		23	 -	?	7.0	4	014.	0	•	
	⋖		30	-	3.	•	-	014.		•	
	⋖		33	-	3	6.7	•	014.	0	•	4
	⋖		93	-	-	7.6	6	020.	6.	•	4
	◂		00	-	7	7.2	œ	020.	0	•	9
	4		03	-	-	7.1	7	020.	0	•	r
	◂		0	-	2.	7.3	څ	019.	<u>د</u>		
	⋖		13	-	2.	7.0	?	019.	•2	•	~
	⋖		20	-	3	7.3	2.	019.	2	•	~
	◁		23	-	?	7.2	3.	018.	٣,	•	\mathbf{c}
	⋖		30	-	2.	7.5	5	018.	~	•	~
	Q		33	-	~	7.5	•	018.	0	•	3
	⋖		0	£	2.	6.4	6	023.	4.		

Table 6,1.1 (continued)

UAY	HONDE	YEAR	TIME	SITE	AT	PPH2G	I &	96	SR	SA	HOM
						108			(M/S0 M)		w
31	⋖	11	3	x	3.	6.0	2	023.	6		
31	◀	11	8	×	4	5.5	•	023.	œ	•	5
31	⋖	11	03	æ	5	5.1	3.	023.	3		~
31	⋖	11	10	×	5.	5.6	4	023.	2.	•	œ
31	Ø	11	13	ĸ	•	5.3	0	023.	٠,		5
31	◀	11	20	æ	5.	6.1	9	023.	7	•	∞
11	⋖	11	22	S	9	7.2	•	021.	7		∞
31	Z V	11	1230	Æ	24.2	17.49	17.1	1022.6	1.31	1.0	166
31	⋖	11	25	v	8	8.5	5	020.	7	•	4
31	⋖	11	30	Œ.	3.	8.0	•	022.	63		5
31	Q	11	32	∽	•	8.3	6	019.	φ.	•	S
31	⋖	11	33	×	3.	8.2	3.	021.	0	•	ĸ.
31	⋖		35	S	7	8.3	80	019.	ပ္	•	5
31	⋖	11	\$	æ	3.	8.0	2	021.	6.	•	'n
31	⋖		45	S	•	8.3	ô	019.	6.	•	\mathbf{r}
77	•		43	-	3	8.4	3.	015.	-	•	~
31	⋖	11	43	Ħ	•	8.2	*	020.	6.	•	5
31	Ø	11	45	S	•	8.3	-	018.	0		S
31	⋖	11	20	-	3.	8.6	4.	015.	6.	•	N
31	⋖	11	50	æ	3.	9.3	4.	019.	&		\$
31	⋖	11	25	S	•	8.2	2	017.	5	•	Ŋ
31	⋖	11	53	-	3.	8.6	00	015.	5		N
31	4	11	53	x	3.	7.7	~	019.	4.		9
31	⋖	21	9	_	3.	8.5	9	014.	5		(1)
-	2	11	90	Æ	-	7.2	•	020.	5	•	~
-	Δ.	11	3	æ	2.	7.3		021.	-		~
-	Q.	7	00	×	~	7.5	•	021.	0	•	9
~	2	11	Ň	S	•	8.8	÷	020.	9		5
-	α.	7	03	-	2.	7.9	-	017.	0		3

Table 6.1.1 (continued)

UAY	HONGE	YEAR	TIME	SITE	AT	PPH20	Ξ	86		SA	HOM
					(DEG)	(TORR)	3	(MBAR)	(M DS/M)	(H/S)	(DEG)
-	0	11	03	I	2.	7.6	5	021.	6.	•	is
-	٠	11	05	S	•	8.7	3.	020.	0.	•	9
-	بر ج	11	10	-	2	7.4		017.	0		~
~	ھ	11	10	×	2.	7.8	•	021.	~		5
-	σ.	11	12	S	•	0	5.	020.	6.	•	4
~	APF	1.1	1130	-	22.3	18.00	89.4	1017.6	1.10	5.4	156
-	۵	11	13	æ	2	7.6	5.	021.	.2	•	5
-	σ.	11	15	S	5	6	6	020.		•	-
-	ã	11	20	-	3.	7.9		017.	-	•	~
-	۵	11	20	æ	3	7.5	3.	021.	.2	•	
~	٥	11	22	S	*	8,1	&	019.	۳.	•	-
-	<u>a</u>	11	23	-	3.	7.7	1.	017.	4		
-	3.	11	23	x	3.	7.1	•	020.		•	
-	Δ.	11	25	S	4.	4.9	9	010.	4	•	O
~	Δ.	11	30	-	3.	7.7	-	016.	• 2	•	
-	0	11	30	Œ	3,	7.4	0	020.	•2	•	0
-	3	11	32	~	*	8.1	8	018.	7.		
· -	۵	11	33	-	3.	7.6	•	016.	0		
~	2	11	33	=	3.	7.3	;	020.		•	0
~	APR	11	35	S	*	8.2	6	018.	0.	•	
~	4	11	40	-	4	8.3	•	015.	0.	•	-
	2	11	6	x	3.	7.9	2	019.	۲.		Ň
~	Δ.	11	42	S	*	9.9	•	017.	6.	•	\blacksquare
-	٥.	11	43	-	3.	8.9	5	015.	6.		~
~	4	11	43	2.	3.	8.1	5.	019.	0	•	3
	2	11	45	S	•	8.8	•	017.	8	•	4
-	۵	11	50	-	3.	9.0	85.7	014.	∞		Ň
-	2	11	50	x	.	8.3	5.	018.	6.		
-	4	11	52	S	ۍ. •	8.9	9	017.	~	•	~

Table 6.1.1 (continued)

×	HINDE	YFAR	TIME	STTE	AT	0 H 2	ĭ	9	Q.	7	107
		· •]	; ; ;	(DEG)	(TORR)	£	(MBAR)	CH/SO H)	(M/S)	(DEC)
~	Ω.	11	~	-	3	8.9	5	014.	-		(
7	2	11	53	X		8.3	5	018.	8		3
~	Δ.	11	55	S	9	9.3	5	017.	• 6	•	4
-	2	11	9	-	3.	9.4	8	014.	•	•	~
~	Δ.	11	93	-	2	7.5		018.			S
~	٥.	11	3	s	\$	8.4	Š	021.	٠,	•	4
7	•	11	9	-	2	7.7	-	018.	6.		5
7	APR	11	1003	S	25.7	18.46	74.3	1021.3	0.89	3.2	149
7	∠	11	03	-	2	7.8	-	018.	0		ø
7	•	11	03	v	5	8.4	4	021.	0.		9
7	σ.	11	10	-	2	8.2	œ	018.	-	•	5
~	2	11	10	S	5.	8.6	4	021.	0		4
~	٥	11	13	-	3.	8.5	8	018.	•	•	4
7	٥.	11	13	∽	•	8.9	5.	020.	۳.	•	r
~	۵	11	20	-	3	8.4	5	018.	7		4
~	۵.	11	20	∽	ţ	8.8	4	020.	7	•	4
7	Φ.	11	23	-	3	8.6	4	017.	5	•	~
7	2	11	23	S	•	8.8	4	020.		•	4
7	•	11	30	-	3.	8.5	4	017.			2
7	Δ.	11	30	S	5.	8.8	5	020	.2	•	3
7	2	11	33	 -	3.	8.6	3.	016.			2
~	σ.	11	33	S	•	8.9	3,	019.	7	•	4
~	2	11	0	-	3.	8.6	3.	016.	0	•	2
~	Δ.	11	0,4	S	•	8.7	3	019.	0		4
~	Δ.	11	43	_	4	9.1	4.	016.	6.		2
~	Δ.	11	43	S	•	8.9	•	018.	6.	•	3
7	۵.	11	50	-	*	8.7	4.	015.	&		~
~	a	11	50	S	•	8.7	2.	018.	6,		4
7	2	77	53	-	4	α. α.	3	015.	۲.		3

Table 6.1.1 (continued)

UAV	HONE	YEAR	TIME	SITE	AT (DEG)	PPH2G (TERR)	R E	BP (MBAR)	SR (W/SQ M)	WS (H/S)	WDH (DEG)
7	•		53	S	•	8.6	2.	018.	00	•	5
7	APR	11	1600	-	24.0	18.84	84.0	1015.7	99.0	6.2	. 35
2	۵.		63	-	3.	8.9	5	015.	.5		3
4	٥		8	~	4	8.5	6	016.	-	•	9
•	۵		\sim	*	2.	7.8	80	016.	6.	•	9
*	۵		5	S	*	8.6	9.	016.	6	•	9
4	0		00	-	2.	8.1	-	013.	9	•	W
4	۵		0	×	5	7.7	•	016.	0	•	9
4	۵		02	S	•	8.5	00	015.	0		9
4	2		03	-	ω. •	8.2	•	013.		•	S
4	۵		03	#	2.	A.	9	016.		•	9
*	م		05	S	•	8.5	8	015.	7		9
4	٥		10	۳	3,	8.3	5	013.	7	•	4
4	0		10	×	2.	4.9	5.	016.	~	•	•
4	۵.		12	S	5	8.	-	015.	-	•	9
*	2		13	-	3	8.1	•	012.	2.	•	•
4	٩		13	ĸ	3.	7.8	•	016.	• 2	•	9
4	<u>~</u>		15	S	5	8.5	-	014.	۲.	•	5
4	2		20	-	3	8.3	4	012.	.2	•	4
4	۵		20	=	3.	7.9	•	215.	•2		S
•	۵.		22	S	3	8.7	œ	014.	~	•	9
4	2		23	 -	3	8.5	5.	011.	.2	•	4
*	٩		23	x	3.	8.2	•	015.	٣,	•	5
4	0		25	S	5	α. α.	6	013.	٠,	•	9
4	2		30	 -	3.	8.5	5.	011.	.2	•	4
4	۵		30	Ħ	٠	8.2	5	014.	.2	•	9
4	٥.		32	S	5	8.7	œ	013.	-	•	9
•	۵		33	-	•	8.5	•	010.	• 2	•	4
•	Q.		33	×	3	2.9	4.	013.	• 2	-	9

Table 6.1.1 (continued)

7	HOPPH	YEAR	TIME	SITE	AT	~		90	SR	S	HOM
					(050)	(TORR)	£	(MBBR)	CH/SO H)	(H/S)	(DEG)
4	2	11	35	w	25.3	8.8	œ	512.	0	•	Ö
4	4	11	6	-	8	8.5	4	010.			5
*	APR	11	1400	=	23.4	18.20	84.4	1013.4	1.16	. 8	162
4	-	11	45	S	5	8.8	•	012.	0	•	9
•	σ.	11	43	-	3.	8.4	•	.600	0		4
4	Q	11	43	X	ë	3.0	3.	013.	0		9
4	a	11	45	S	5	8.6	9	011.	6.	•	Ó
4	0	11	50	-	m,	8.5	3.	.600	6.	•	5
4	٩	11	20	x	3	8.0	3.	012.	0	•	ø
*	Э.	11	52	S	5	8.6	-	011.	-	•	9
4	Q.	11	53	=	3.	8.1	3.	012.	Φ.	•	9
S.	a	11	93	-	*	7.8	8	.600	80		œ
2	2	11	8	S	8	7.5	-			•	
S	Δ.	11	03	S	•	7.0	•			•	
5	٥.	11	10	S	•	5.9	6			•	
ß	٥.	11	13	S	,	6.0	•	013.	•	•	3
S	۵.	11	20	S	-	5.1	*	013.	4.		~
S	2	11	23	S	•	5.0	3.	012.	.5	•	~
v	Δ.	11	30	S	5	4.4	œ	013.	0		9
S	α.	11	3	S		3.8	8	1014.3	0.36	•	292
S	Δ.	11	0	S	÷	2.3	•	014.	8		$\boldsymbol{\Phi}$
S	2	11	43	S	5.	2.2	•	014.	6.	•	∞
S	α.	11	20	S	5.	0.8	•	013.	4.		9
S	•	11	53	S	•	6.	1.	013.	.5	- •	9
•	2	11	10	-	8	7	5.	023.	6.		3
9	•	11	13	-	•	•	5.	023.	6.		σ
9	۵.	1.1	20	-	7.	6.	5	023.	.2		4
9	٥	11	23	þ- -	8	0	5.	022.	6.	•	~
9	Φ.	11	40	۲	80	0	5.	022.	~		0

Table 6.1.1 (continued)

UAY	INDE	YEAR	TIME	SITE	AT	PPHZG	I	86	SR	N.S	HOM
					(DEG)	TOR	€			(W/S)	(DEG)
•	APR	77	1430	٠.	~		S		1.02	4.5	153
9	APR	11	50	_	æ	0	5.	021.	6.		ø
9	APR	11	53	-	80	6	8	021.	æ	•	
•	APR	11	0	-			•	021.	0.76	•	
9	APR	11	63	-	-	.2	-	021.	5	•	
_	APR	11	00	-	-	5	4		8		
~	APR	11	03	-	-	۳.	-		•		
~	APR	11	10	-					0		
~	APK	11	13	-					1.		
~	APR	11	20	-					7		
~	APR	11	23	 -					-2		
~	Ā	11	30	۳							
~	200	11	33	-							
~	APR	11	40	-					7.		
~	APR	11	43	-					0		
	MAY	11	42	S	5	4.4	6	82.	2.	•	2
	MAY	11	45	S	5.	5.3	3.	91.	-2	•	0
	MAY	77	52	S	5	5.5	4	78.	7.	•	0
	MAM	11	55	S	5	5.4	9	76.	0	•	
	* 5 2	11	62	S	5	5.3	2.	76.	6.	•	0
	702	11	65	S	\$	5.3	2.	974.	80	•	0
	MAY	11	8	S	5.	8.0	3	024.	8	•	~
	A D E	11	03	~	5	8.1	•	24.	• 6		
	Y V X	11	10	S	5	8.2	3.	984.	0	•	
	Y U E	11	13	S	5	7.4	-	79.		•	
11	× V W	11	20	S	25.4	17.22	70.6	978.4	.2	5.7	7.5
	N A M	77	23	S	5.	7.0	9.	78.	.2	•	
	MAM	11	9	S	5.	6.7	8	76.	(1)		
	* Q #	77	33	~	5	6.2	•	74.	~	•	

Table 6.1.1 (continued)

77 1400 S 25.7 16.29 65. 77 1430 S 25.5 16.13 65. 77 1500 S 25.7 16.13 65. 77 1630 S 25.7 15.71 63. 77 1690 S 25.9 15.40 61. 77 1630 S 26.1 15.89 62. 77 958 S 26.0 15.89 62. 77 1058 S 26.0 15.45 61. 77 1033 S 26.0 15.45 61. 77 1033 S 26.3 15.53 60. 77 1033 S 27.6 14.43 57. 77 1103 S 27.6 14.44 57. 77 1233 S 26.7 14.46 55. 77 1403 S 26.7 14.23 57. 77 1603 S 26.0 14.90 56. 77 <th>R) (%) (MB</th> <th>アウトライ へくる</th> <th>M) (M/S)</th> <th>(DEG)</th>	R) (%) (MB	アウトライ へくる	M) (M/S)	(DEG)
7 1430 S 25.5 16.13 65 7 1500 S 25.6 16.13 65 7 1600 S 25.7 15.40 61 7 1630 S 25.9 15.40 61 7 1630 S 26.1 15.89 62 7 1028 S 26.1 15.89 62 7 1028 S 26.0 15.53 62 7 1058 S 26.0 15.53 62 8 26.2 15.69 61 61 958 S 26.0 15.53 62 1 1033 S 26.2 15.69 61 1 1033 S 27.6 14.46 55 1 1033 S 27.6 14.66 56 1 1033 S 26.7 14.23 57 1 1403 S 26.7 14.96 56 1 1603 S 26.8 <t< th=""><th>6 6.29</th><th>.2 1.3</th><th>•</th><th></th></t<>	6 6.29	.2 1.3	•	
1500 S 25.6 16.13 65 7 1500 S 25.7 15.71 63 7 1600 S 25.9 15.40 61 7 1630 S 25.9 15.51 62 7 1700 S 26.1 15.89 62 7 1028 S 25.9 15.89 62 7 1028 S 26.0 15.53 62 7 1058 S 26.0 15.45 61 7 1068 S 26.0 15.45 61 7 1033 S 26.3 15.53 60 7 1033 S 27.4 14.44 55 7 1103 S 27.4 14.46 55 7 1103 S 27.4 14.46 55 7 1203 S 26.7 14.23 55 7 1403 S 26.7 14.96 56 7 1603 S <t< th=""><th>65</th><th>.1 1.3</th><th>5.3</th><th></th></t<>	65	.1 1.3	5.3	
7 1530 S 25.7 15.71 63 7 1600 S 25.9 15.40 61 7 1630 S 26.1 15.89 62 7 1700 S 26.1 15.89 62 7 1028 S 26.0 15.89 62 7 1028 S 26.0 15.89 62 7 1038 S 26.0 15.85 61 7 1038 S 26.3 15.69 61 7 1033 S 26.3 15.69 61 7 1103 S 27.0 14.46 55 7 1103 S 27.4 14.46 55 7 1233 S 26.9 14.23 55 7 1433 S 26.7 14.86 56 7 1433 S 26.8 14.90 56 7 1603 S 26.8 14.90 56 7 1603 <t< th=""><th>6 5.4 9</th><th>.9 1.2</th><th>•</th><th></th></t<>	6 5.4 9	.9 1.2	•	
7 1600 S 25.9 15.40 61 7 1630 S 26.1 15.89 62 7 928 S 26.1 15.89 62 7 928 S 26.0 15.53 62 7 1028 S 26.0 15.55 61 7 1028 S 26.0 15.55 61 7 1038 S 26.0 15.69 61 7 1033 S 26.3 15.53 60 7 1103 S 27.0 14.71 55 7 1103 S 27.0 14.43 57 7 1133 S 27.0 14.46 50 7 1233 S 26.9 14.46 50 7 1333 S 26.9 14.23 53 7 1433 S 26.0 14.96 56 7 1603 S 26.0 14.96 56 7 1603	63.4	.1 1.1	•	
7 1630 S 26.1 15.51 61 7 1700 S 26.1 15.89 62 7 928 S 26.0 15.53 62 7 1028 S 26.0 15.55 61 7 1028 S 26.0 15.55 61 7 1058 S 26.2 15.69 61 7 1033 S 26.2 15.69 61 7 1103 S 27.0 14.71 55 7 1103 S 27.0 14.64 50 7 1133 S 27.0 14.46 50 7 1233 S 27.0 14.64 50 7 1303 S 26.0 14.0 50 7 1403 S 26.0 14.0 50 7 1433 S 26.0 14.90 56 7 1603 S 26.0 14.90 56 7 1603 S	61.6	.4 1.0	•	
7 1700 S 26.1 15.89 62 7 958 S 26.0 15.55 61 7 1028 S 26.0 15.55 61 7 1028 S 26.0 15.45 61 7 1058 S 26.2 15.69 61 7 1033 S 27.0 14.71 55 7 1133 S 27.5 14.65 54 7 1233 S 27.5 14.23 57 7 1233 S 27.5 14.23 57 7 1333 S 26.7 14.67 55 8 14.35 S 26.9 14.86 56 8 16.36 S 26.8 14.90 56 8 16.36 S 26.8 14.90 56 8 16.36 S 26.8 14.90 56 8 16.36 S 26.8 16.36 64 8 1131 S 26.2 16.36 64	61.19	6.0 7.		
7 928 S 26.0 15.53 62 7 1028 S 26.0 15.45 61 7 1058 S 26.2 15.69 61 7 1058 S 26.2 15.69 61 7 1003 S 27.0 14.71 55 7 1103 S 27.4 14.43 57 7 1133 S 27.5 13.82 50 7 1233 S 27.5 14.23 57 7 1333 S 26.9 14.23 53 7 1403 S 26.9 14.23 53 7 1503 S 26.9 14.90 56 7 1503 S 26.9 14.90 56 7 1503 S 26.8 14.90 56 7 1503 S 26.8 14.90 56 7 1503 S 26.8 16.36 64 7 1101 S 26.2 16.36 64	65.5	9.0 9.	•	
7 1028 S 26.0 15.55 61 7 1028 S 26.2 15.69 61 7 1058 S 26.3 15.53 60 7 1003 S 27.0 14.71 55 7 1033 S 27.4 14.65 54 7 1133 S 27.6 14.10 50 7 1233 S 27.5 13.82 50 7 1233 S 26.9 14.23 53 7 1303 S 26.9 14.23 53 7 1503 S 26.9 14.23 53 7 1503 S 26.9 14.29 55 7 1503 S 26.9 14.90 56 7 1503 S 26.9 14.90 56 7 1503 S 26.9 14.90 56 7 1503 S 26.8 14.90 56 7 1503 S 26.8 16.36 64 7 1101 S 26.2 16.36 64	62.3 10	.7 0.6	•	
7 1028 \$ \$ 56.0 15.45 61 7 1058 \$ \$ 26.2 15.59 60 7 1003 \$ \$ 26.3 15.59 60 7 1003 \$ \$ 27.0 14.71 55 7 1103 \$ \$ 27.4 14.65 54 7 1103 \$ \$ 27.4 14.65 56 7 1133 \$ \$ 27.6 14.43 57 7 1233 \$ \$ 26.9 14.23 59 7 1303 \$ \$ 26.7 14.67 55 7 1403 \$ \$ 26.7 14.67 55 7 1403 \$ \$ 26.7 14.86 56 7 1433 \$ \$ 26.7 14.96 56 7 1603 \$ \$ 26.8 14.90 56 7 1603 \$ \$ 26.8 <th>61.6 10</th> <td>8.0 6.</td> <td></td> <td></td>	61.6 10	8.0 6.		
7 1058 S 26.2 15.69 61 7 1128 S 26.3 15.53 60 7 1003 S 27.0 14.71 55 7 1033 S 27.4 14.43 57 7 1133 S 27.6 14.43 57 7 1203 S 27.6 14.43 57 7 1233 S 26.9 14.23 53 7 1303 S 26.9 14.23 53 7 1403 S 26.7 14.86 56 7 1403 S 26.7 14.96 56 7 1503 S 26.8 14.90 56 7 1603 S 26.8 14.90 56 7 1603 S 26.0 16.36 64 7 1131 S 26.2 16.36 64 7 1131 S 26.2 16.36 64	61.2 10	.1 0.7	•	
7 1128 S 26.3 15.53 60 7 1003 S 27.0 14.71 55 7 1033 S 27.1 14.65 54 7 1103 S 27.4 14.65 55 7 1133 S 27.6 14.10 50 7 1233 S 27.5 13.82 50 7 1233 S 26.9 14.23 53 7 1333 S 26.7 14.67 55 7 1433 S 26.6 14.96 56 7 1433 S 26.6 14.96 56 7 1503 S 26.8 14.90 56 7 1603 S 26.8 14.90 57 7 1031 S 26.2 16.36 64 7 1131 S 26.2 16.36 64	61.6 10	.2 1.1	•	
7 1003 S 27.0 14.71 555 7 1033 S 27.1 14.65 54 7 1103 S 27.4 14.43 57 7 1203 S 27.6 14.10 50 7 1233 S 27.5 13.82 50 7 1303 S 26.9 14.23 53 7 1403 S 26.7 14.67 55 7 1403 S 26.6 14.96 56 7 1503 S 26.8 14.90 56 7 1503 S 26.8 14.90 56 7 1503 S 26.8 14.90 56 7 151 S 26.0 16.11 63 7 1101 S 26.2 16.36 64	60.4 10	.3 1.1		
7 1033 S 27.1 14.65 54 7 1103 S 27.4 14.43 52 7 1203 S 27.5 14.10 50 7 1203 S 27.5 13.82 50 7 1203 S 27.5 14.18 52 7 1303 S 26.9 14.23 53 7 1403 S 26.7 14.67 55 7 1403 S 26.8 14.90 56 7 1503 S 26.8 14.90 56 7 1503 S 26.8 14.92 56 7 1003 S 26.2 16.36 64 7 1131 S 26.2 16.36 64	55.0 10	.5 0.8	•	0
7 1103 S 27.4 14.43 52 7 1133 S 27.6 14.10 50 7 1233 S 27.5 13.82 50 7 1233 S 21 14.18 52 7 1333 S 26.9 14.23 53 7 1403 S 26.7 14.78 55 7 1503 S 26.6 14.90 56 7 1533 S 26.8 14.90 56 7 1533 S 26.8 14.90 56 7 1533 S 26.8 16.30 57 7 1031 S 26.2 16.36 64 7 1131 S 26.2 16.36 64	54.4 10	6.0 9.	•	
7 1133 S 27.6 14.10 50 7 1233 S 27.5 13.82 50 7 1233 S 21 14.18 52 7 1333 S 26.9 14.23 53 7 1403 S 26.7 14.67 55 7 1403 S 26.7 14.78 56 7 1503 S 26.8 14.90 56 7 1533 S 26.8 14.90 56 7 1631 S 26.8 14.92 56 7 1031 S 26.2 16.36 64 7 1131 S 26.2 16.36 64	52.7 10	.8 1.0	•	0
7 1203 S 27.5 13.82 50 7 1233 S 2 14.18 52 7 1303 S 26.9 14.23 53 7 1303 S 26.7 14.67 55 7 1403 S 26.7 14.78 56 7 1503 S 26.8 14.90 56 7 1503 S 26.8 14.90 56 7 1603 S 26.8 14.92 56 7 1011 S 26.2 16.36 64 7 1131 S 26.2 16.36 64	50.8 10	.9 1.1	•	6
7 1233 S 24.91 14.18 52 7 1303 S 26.9 14.23 53 7 1303 S 26.7 14.67 55 7 1403 S 26.7 14.78 56 7 1503 S 26.6 14.90 56 7 1503 S 26.8 14.90 56 7 1603 S 26.8 14.92 56 7 1031 S 26.0 16.11 63 7 1101 S 26.2 16.36 64 7 1131 S 26.2 16.37 63	50.1 10	.9 1.2	•	
7 1303 S 26.9 14.23 53 7 1333 S 26.7 14.67 55 7 1403 S 26.7 14.78 56 7 1503 S 26.8 14.90 56 7 1503 S 26.8 14.90 56 7 1603 S 26.8 14.92 56 7 1031 S 26.0 16.11 63 7 1101 S 26.2 16.36 64 7 1131 S 26.2 16.36 64	52.6 10	.8 1.2	•	
7 1333 S 26.7 14.67 55 7 1403 S 26.7 14.78 56 7 1503 S 26.8 14.90 56 7 1503 S 26.8 14.90 56 7 1533 S 26.8 14.92 55 7 1603 S 26.8 15.20 57 7 1031 S 26.2 16.36 64 7 1131 S 26.2 16.36 64	53.6 10	.8 1.3	•	
7 1403 S 26.7 14.78 56 7 1433 S 26.6 14.86 56 7 1503 S 26.8 14.90 56 7 1533 S 26.8 14.92 55 7 1603 S 26.8 15.20 57 7 1031 S 26.0 16.11 63 7 1101 S 26.2 16.36 64 7 1131 S 26.2 16.37 63	55.9 10	.5 1.3		
7 1433 S 26.6 14.86 56 7 1503 S 26.8 14.90 56 7 1603 S 26.8 14.92 56 7 1603 S 26.8 15.20 57 7 1031 S 26.0 16.11 63 7 1101 S 26.2 16.36 64 7 1131 S 26.2 16.17 63	56.1 10	.7 1.2	•	
7 1503 S 26.8 14.90 56 7 1533 S 26.8 14.92 56 7 1603 S 26.8 15.20 57 7 1031 S 26.0 16.11 63 7 1101 S 26.2 16.36 64 7 1131 S 26.2 16.17 63	56.9 10	.5 1.2	•	
7 1533 S 26.8 14.92 56 7 1603 S 26.8 15.20 57 7 1031 S 26.0 16.11 63 7 1101 S 26.2 16.36 64 7 1131 S 26.2 16.17 63	56.4 10	.6 1.1	•	
7 1603 S 26.8 15.20 57 7 1031 S 26.0 16.11 63 7 1101 S 26.2 16.36 64 7 1131 S 26.2 16.37 63	56.6 10	.4 1.0	•	
7 1031 S 26.0 16.11 63 7 1101 S 26.2 16.36 64 7 1131 S 26.2 16.17 63	57.6 10	.0 1.0	•	
7 1101 S 26.2 16.36 64 7 1131 S 26.2 16.17 63	63.7 10	6.0 4.	•	
7 1131 5 26.2 16.17 63	64.2 10	0.1 9.		
£7 0£ 71 € 76 3 10€1 €	63.3 10	.1 1.1	•	
60 96.01 6.02 8 1021 1	63.9 10	0.2 1.22	5.0	9 5

Table 6.1.1 (continued)

UAY	HON	YEAR	TIME	SITE	AT (DEG)	PPH2G (TGRR)	# E	BP (MHAR)	SR (W/SQ M)	HS (M/S)	WDH (DEG)
21	•	17	1231	S	•	6.2	3.	60	-2	•	0
7.7	⋖	11	0	S	•	6.5		019.	•2		
2.1	•	11	33	S	•	6.4	+	019.	4.	•	0
21	₫	11	9	S	5	6.7	-	019.	• 5	•	9
77	₫	11	4 3	S	9	9.9	5.	019.	6.	•	
21	•	11	50	S	•	6.7	۴.	019.	• 2	•	Œ
23	◂	11	93	S	9	8.1	6	016.	•	•	Ę
23	a	11	00	S	7.	8.2	5	16.	œ	•	
23	q	11	03	~	7.	7.7	5.	016.	Ç	•	\sim
23	◂	11	10	S	8	7.6	-	015.	3	•	٥
73	d	11	13	S	5	7.7	2	016.	0.	•	-
53	•	11	20	S	5.	7.9	-	016.	4.	•	œ
53	⋖	11	23	S	5	7.9	2.	016.	*	•	~
23	⋖	11	30	S	9	7.4	5.	015.	*	•	3
53	•	11	33	S	•	7.5		015.	۲.		-
23	q	11	6	S	•	7.6	&	015.	•	•	œ
67	⋖	11	43	S	9	7.9	0	968.		•	
53	•	11	50	V.	•	9.2	2	67.	£.	•	
23	Œ	11	53	S	9	8.3	3.	71.	•	•	
73	. V W	11	0	S	26.2	18.55	72.8	971.	1.13	3.5	я 3
63	•	11	63	S	• 9	R. 7	~	14.	0		0
54	◂	11	83	S	•	1.1	2	016.	•2	•	œ
47	◂	11	0	S	~	1.2	7.	016.	ر •	•	9
57	Œ	11	93	S	œ	1.3	5	016.	•		9
24	⋖	11	07	S	-	0.5	•	960.	۲.	•	~
47	◂	11	13	S	•	0.3	• 9	017.	• 2		~
54	Ø	11	C	<u>~</u>	•	0.2	•	17.	3	•	
47	◂	11	23	v	•	0.0	•	017.	4.	•	~
5 ?	<	11	30	S	9	0.2	8	960.	4.	•	~

Table 6.1.1 (continued)

UAY	I P D I	YEAR	TIME	SITE	AT (DEG)	PPH2G (TORR)	## ##	BP (MBAR)	SR (W/SQ M)	WS (M/S)	WDH (DEG)
24		7.7	1331	S	26.4	20.57	19.8	462.4	1.62	C	114
54		11	1401	S	26.4	20.59	79.6	1016.9	1.30	. u	711
24		11	1431	S	26.5	20.89	80.5	1016.6	000	2	1 1 2
54		11	1501	S	26.8	20.94	79.1	1016.0	1.44		133
57		11	1532	S	26.7	21.10	80.2	1015.9		• 0	118
25		11	903	S	27.8	20.83	74.7	1015.1	9.5.0	2,6	212
25		11	933	S	28.9	20.12	67.4	1015.1	0.73	7.	228
25	MAY	11	1003	S	30.0	19.97	62.8	1015.2	0.60	2.6	747
25		11	1033	S	31.5	18.57	53.7	1014.9	1.00		× × ×
25		11	1103	S	32.4	17.30	47.6	1015.0	1.12	1.7	219
52		11	1133	S	30.5	20.07	61.2	1015.0	1.24		145
52		11	1203	S	29.9	20.17	65.8	1014.8	1,33	0	150

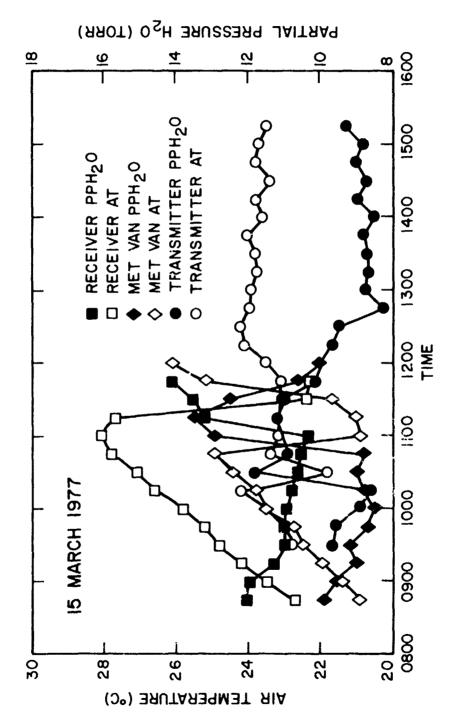


FIG. 6.1.1. AIR TEMPERATURE AND PARTIAL PRESSURE OF WATER VAPOR MEASURED AT THE THREE SITE LOCATIONS ON 15 MARCH 1977.

6.236-02 7.696-02 6.726-02 6.116-02 1.07E-01 1.17E-01 2.17 (EE) 2.966-01 3.02E-01 2.81E-01 4.52E-01 2.026-01 2.026-01 2.236-01 2.036-01 2.056-01 2.156-01 3.086-01 3.416-01 1.22 Particle Density (1/cc/um) vs. Particle Radius NRL Aerosol Size Distribution Measurements 55 33 Table 6.2.1 55 5666 55 9.22 55 322 25 20.00 1115 3558 0.12

7.7

28 FFB

ADTUS

3.12

				NRL / Particle	Ta Aerosol e Density	able Size y (1/	.2.1 Distr c/µm)	<pre>1 (Continued tribution Mea m) vs. Parti-</pre>) asur cle	ഗഗ	(mn)		
X A	KADIUS .	î	5.02	5.97	26.0	7.87	8. 82	9.17	10.12	11.67	12.62	13.57	14.52
28 F	FEB 77	1430	1.916-03	4.78E-04 1.375-03	1.142-03	4.786-04	5.376-64 1.796-04	1.196-04	0.00E 00 5.97E-05	0.00F 00 0.00E 00	5.97E-05 0.00E 00	0.00£ 00 0.00£ 00	0.00£ 00
-	MAR 77	7 1100 1130 1200 1233	5.976-04 7.165-04 4.785-04 4.786-04	6.57E-04 5.37E-04 1.79c-04 1.79E-04	6.276-04 3.596-04 7.986-04 5.976-05	2.93E-04 1.19E-04 1.19E-04 1.79E-04	1.19E-04 4.18E-04 0.00E 00 5.37E-05	5.97E-05 5.97E-05 5.97E-05 0.00E 03	0.00E 00 0.00E 00 0.00E 00	1.79E-04 5.97E-05 0.00E 00	1.196-04 0.006 00 0.006 00	0.00E 00 0.00E 00 0.00E 00	0.00£ 00 0.00£ 00 0.00£ 00
~	7 A A A 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	\$ 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4.78E-04 1.79E-04 5.97E-05 6.98E-04 6.98E-04 1.79E-04 1.7	2.992-05 0.006 0.006 0.006 0.006 1.96-03 1.196-04 1.976-04 1.976-04 2.976-05	2.98f-04 2.98f-04 5.00f-05 5.97f-05 5.97f-05 5.97f-04 5.97f-04 1.79f-04		0.00E 0.00E 0.00E 0.00E 0.00E 0.00E 0.00E 0.00E 0.00E 0.00E	5.416-05 0.006-05 5.906-05 0.006-05 0.006-05 0.006-05 0.006-05 0.006-05 0.006-05 0.006-05	0.006 0.006 0.006 0.006 0.006 0.006 0.006 0.006 0.006 0.006 0.006 0.006 0.006 0.006	00.006 00.006 00.006 00.006 00.006 00.006 00.006 00.006 00.006 00.006 00.006 00.006	0.00 E 00 0.00 E 00	00000000000000000000000000000000000000	000000000000000000000000000000000000000
# m	7 X 4 8 7 7 7		7.566 9.366 9.366 9.366 7.368 9.368 9.368 11.02	7.7. 4.166 4.166 3.866 6.766 6.776 6.7		5.09 fc			2000 1000 0000 0000 0000 0000 0000 0000	2000 2000			5.94 E . 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 .
# →	7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7			9 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		\$ 50 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0							55-98-98-98-98-98-98-98-98-98-98-98-98-98-
•	MAR 77			7.585-02 4.235-02 5.295-02	3.87E-02 1.95E-02	1.416-92 9.736-03	****				8.36E-04 2.39E-04 5.97E-04	2.39E-04 2.98E-04 7.76E-04	1.19E-04 1.79E-04 1.79E-04

	***	1.52E-01 1.55E-01 1.58E-01 2.16E-01 2.56E-01	2 · 4 3E · 0 1 2 · 6 5 6 · 0 1 2 · 3 2E · 0 1	8.176-01 9.046-01 5.40E-01 3.246-01	2.552. 1.652. 1.652. 1.652. 1.652. 1.652. 1.652. 1.653. 1.	2.546-03 2.576-03 2.156-03 1.856-03 2.266-03 2.266-03 3.166-03 2.266-03 3.166-03 5.576-03
	3.12	5.786-01 5.526-01 7.516-01 8.766-01	8.22E-01 4.55E-01 7.91E-01 5.63E-01 9.36E-01	3.026 00 3.466 00 1.946 39	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1.79E-02 2.72E-02 2.72E-02 2.72E-02 2.72E-02 1.74E-02 1.75E-02 2.16E-02 2.16E-02 2.16E-02 2.16E-02 2.16E-02 2.16E-02 3.16E-02 4.00C-02
(mn)	2.17	1.586 00 1.586 00 1.626 00 1.956 00	2.224 00 2.384 00 1.366 00 2.16 00 1.786 00 1.988 00 2.516 00	6.93E 00 8.54E 00 5.33E 00 3.34E 00	1.64E 1.57F	2
10 10	1.22	5.19E 00 4.52E 00 4.11E 00 5.02E 00 5.20E 00	1.086 01 9.746 00 9.256 00 9.256 00 8.046 00 1.296 01	2.296 01 3.316 01 1.976 01 1.356 01	5.59 6 00 5.69 6 00 5.60 6 00	2.5394 E 00 C 2.5394 E 00 C C C C C C C C C C C C C C C C C
) asur cle	0.33	9.25E 01 8.82F 01 8.97E 01 8.60E 01	4.15E 02 3.35E 02 4.15E 02 4.05E 02 4.37E 02	2.186 02 3.906 92 2.65£ 02 1.91£ 02	3.55£ 01 5.55£ 01 5.55£ 01 5.55£ 01 5.55£ 01 5.55£ 01 5.55£ 01 5.55£ 01 6.55£ 01 6.55£ 01 6.55£ 01 6.55£ 01	3.474 01 11.474 01 11.624 01 11.624 01 11.624 01 11.624 01 11.624 01 11.624 01 11.634 01 11.64 01 11.64 01
ntinu Eion . Par	0.29	9.39E C1 1.23E O2 7.34E 91 1.60E 02	7.40E 5.20E 5.60E 5.60E 6.30E 6.30E 6.30E 6.31E 6.31E 6.31E	3.516 62 4.546 92 2.556 92 2.336 92		2.02.00 2.02.00 2.02.00 2.02.00 2.02.00 2.02.00 2.02.00 2.02.00 2.03.0
6.2.1 (Come Distribution) /cc/µm) vs	0.26	2.29E 02 2.54E 02 2.29E 02 3.77E 02 3.53E 02	1.21E 03 8.46E 02 1.07E 03 8.59E 02 9.40E 02 1.38E 03	5.17E 02 8.40E 02 4.69E 02 3.94E 02	7.00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2.00 4 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
ble Siz (1	9.25	4.20E 32 4.49E 62 5.81E 02 5.89E 02	2.456 03 1.516 03 1.516 03 1.376 03 1.536 03 1.576 03 1.706 03	8.17E 02 1.35E 03 7.86E 02 7.51E 92	2.038 2.	2.64% 011 2.64%
Aercol Densit	6.19	1.416 03 4.70c 43 1.446 53 1.866 93 2.636 93	5.37c .3 4.49c .3 3.94c .3 4.63c .3 4.17c .3 4.25c .3 3.97c .3 4.25c .3	2.34E 93 4.31, 03 4.37E 93 1.90E 93	66.3416 66.3417 66.	60000000000000000000000000000000000000
Ta NRL Aercrol Particle Density	9.15	1.64E 93 1.72E 93 1.56E 63 2.21E 93 2.16E 03	5.20E 03 3.60E 03 4.37E 03 4.00E 03 4.14E 03 3.71E 03 3.71E 03	2.41E 03 5.69E c3 2.65E 03 2.05E 03	56. 446 92 93 94 94 94 94 94 94 94 94 94 94 94 94 94	11.0046 99.0046 99.0046 99.0046 99.0046 99.006 99.006 99.006 99.006 99.006 99.006
-	6.12	**************************************	9.426 9.426 9.426 9.436 9.436 9.436 9.436 9.436 9.436 9.436 9.436 9.436 9.436	1.476 34 1.476 34 8.315 33 4.25 63	2.00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	3.975.02 3.716.02 3.716.02 3.716.02 3.716.02 2.675.02 2.675.02 2.675.02 2.876.02 2.876.02 2.876.02
	c sn	R 77 11130 1200 1230 1300 1330	77 4900 10000 10000 11000 11100 1200	R 77 930 1000 1030 1100	74 9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	A 77 100000 100000
	RADIUS	4 A A A	OI MAN	T T	12 MAN	4 * * * * * * * * * * * * * * * * * * *

vs. Particle Radius NRL Aerosol Size Distribution Measurements Table 6.2.1 (Continued) Particle Density (1/cc/um) 2.296-01 2.456-01 1.296-01 7.896-02 3.18E-01 3.40E-01 2.63E-01 1.20E-01 11 11 2 RADIUS MAR * # * 2 2

					NRL Particl	NRL fc16	٠ م	Ta lerosol Density	Table (1) Size (1)	a 🔨	6.2.1 Dist cc/µm	SH ((Continued) ibution Mea	inu on Par	inued) on Meas Particl	ure e R	.2.1 (Continued) Distribution Measurements c/µm) vs. Particle Radius	(E m)	(H		
RAC	AADIUS -	î	0.12	~	0.15	•	0.19	•	0.22	~	0.26	.0	ò	0.29	٥	0.33	1.22	~	2.17	3.12	4.07
±	17 MAN 77	1530 1600 1600 1700 1730	3.316 3.776 4.296 3.606	22222	9.03E 9.03E 9.03E	00000	5.80E 7.37E 7.26E 9.66E	22020	2.89E 2.32E 2.55E 2.55E	55555	3.20E 2.84E 2.89E 2.27E	55555	1.45E 2.84E 1.74E 3.69E	25555 25555	2.806 7.456 1.526 2.486	26 01 26 01 36 01 36 01	2.78E 2.72E 2.79E 2.79E 2.79E	80000	4.66E-01 4.40E-01 4.59E-01 4.33E-01	4.03E-02 3.29E-02 3.8E-02 3.03E-02	4.546 3.466 4.8466 6.3466 6.3466 6.3466 6.00 6.00 6.00 6.00 6.00 6.00 6.00 6
2	MAR 77	1000 1000 1000 11000 11300 1200	6.20 10.20 10.20 10.00 1	0000000	2.94 2.54 2.54 3.54 1.54 1.54	0000000	1.25 1.196 1.196 1.656 1.036	222222	4.5.46 4.5.46 5.846 6.86 6.86 6.86 6.86 6.86 6.86 6.86	5555555	2.2.2 2.2.2 2.2.2 4.3.2 4.3.4 6.3.4	222222	2.56 2.55 3.65 3.65 3.65 6.65 6.65 6.65 6.65 6	2222222	11.00.00 10.00 10.00.00 10.00.00 10.00.00 10.00.00 10.00.00 10.00.00 10.00.	26 01 76 01	1.94 E 1.95 E 2.79 E 3.00 E	0000000	2.926-01 2.816-01 2.836-01 7.946-01 7.976-01	1.0496 1.0496 1.0496 1.056 1.056 1.056 1.056 1.056 1.056	2.00 2.00 2.00 2.00 2.00 2.00 2.00 2.00
E E	MAR 77	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4				22 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		00 00 00 00 00 00 00 00 00 00 00 00 00		2222222222222		777777777777777777777777777777777777777	2月 まるみようゆうできらりりままます。。。。。。。。。。。。。。。。。。。。。。。。。。。。。。。。。		2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	000000000000000000000000000000000000000	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	000000000000000000000000000000000000000	3.286 01 3.126 01 1.736 01 1.736 01 1.806 01 5.17 01 5.76 01 5.76 01 5.96 01 5.86 01 6.36 01	4.19E-02 3.18E-02 1.19E-02 1.19E-02 1.06E-02 2.33E-02 1.33E-01 1.33E-01 1.53E-01 1.53E-01 1.59E-01 1.69E-01	5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0
	# # # # # # # # # # # # # # # # # # #		44444444444444444444444444444444444444		20 20 20 20 20 20 20 20 20 20 20 20 20 2					222222222222		000000000000000000000000000000000000000	2 2 3 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		7.200 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	05 05 05 05 05 05 05 05 05 05 05 05 05 0	2000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	000000000000000000000000000000000000000	9.22 9.22 7.45 6.35 6.34 6.34 6.34 6.34 6.34 6.34 6.34 6.34	3.28E-01 2.5.4E-01 2.5.5 01 2.5.5 01 1.92E-01 1.92E-01 1.92E-01 1.92E-01 1.67E-01 1.67E-01 1.67E-01	7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7
~ *	APR 17	11000	3.57E 3.57E 3.09E	5 3536	7. 71E 1. 855 1. 36E	2 555	1.39E 1.03E 9.91E	2 55 55	3.4.2 2.40 2.48 2.47	7777	5.77E 1.75E 1.55E	770	3.71E 6.03E 9.13E	0 000	3.10E 7.02E 5.02E	0E 01 2E 01 0E 01	2.976 3.606 3.896 3.896	0 0000	7.986-01 9.346-01 1.026-00 9.426-01	2.08E-01 2.71E-01 2.76E-03 2.54E-01	7.55E-02 8.15E-02 9.15E-02

		NRL Particl	Tal L Aerosol le Density	ble Size (1/	6.2.1 (CDistribution of the complex	.1 (Continued) stribution Measurement µm) vs. Particle Radiu	inued) on Measuren Particle Ra	ഗ ഗ	(mn)		
RADIUS>	5.02	5.97	6.92.	7.87	8.82	9.11	10.72	11.67	12.62	13.57	14.52
14 MAR 77 1530 1600 1700 1700 1730	8.36E-04 1.07E-03 5.97E-04 9.55E-34	4-18:-04 5-37:-64 2-39:-04 4-18:-04 5-97:-04	1.796-04 2.396-04 4.786-04 5.986-04	2.39E-04 C.U3E-03 3.58E-04 3.58E-05	1.196-04 3.586-04 1.196-04 1.196-04 5.976-05	5.97E-05 0.30E-05 5.97E-05 1.19E-04 5.97E-05	0.00E 00 0.00E 00 5.97E-05 0.00E 00 1.19E-04	5.97E-05 0.00E 00 0.00E 00 0.00E 00	5.376-05 0.00E 00 0.00E 00 0.00E 00	0.00E 00 0.00E 00 0.00E 00 0.00E 00	0.00E 0.00E 0.00E 0.00E 0.00E
15 MAR 77 900 930 1700 11030 11030 1209	1.016-03 1.076-03 8.366-04 4.186-04 1.576-02	1.676-03 1.43E-03 1.19E-03 8.36E-04 7.16E-03 1.26E-02	1.376-03 2.336-03 1.256-03 1.436-03 3.586-03 6.446-03	1.736-03 2.346-03 8.366-04 1.146-03 1.256-03 3.766-03	7.16E-04 8.95E-04 5.37E-04 5.37E-04 2.08E-04 7.16E-04	8.36E-04 1.25E-03 5.37E-04 4.18E-04 4.78E-04 1.25E-03	5.97E-04 2.98E-04 2.98E-04 1.79E-04 4.18E-04	2.396-04 1.196-04 0.006-00 5.976-05 2.986-04	0.00E 00 5.97E-05 0.00E 00 0.00E 00 1.79E-04	0.00E 00 0.00E 00 0.00E 00 0.00E 00 1.19E-04	0.00E 00 0.00E 00 0.00E 00 0.00E 00 0.00E 00
31 MAR 77 900 1000 1100 11100 1130 1230 1230 1230 1	3.44E-03 2.03E-03 5.97E-04 4.18E-04 1.185E-0 2.11E-02 2.74E-02 2.74E-02 2.74E-02 2.74E-02	1. 196 - 03 9. 356 - 03 3. 356 - 04 1. 196 - 04 7. 76 - 04 1. 176 - 02 1. 176 - 02 1. 186 - 02	7.76E.004 22.396E.004 22.396E.004 23.996E.004 23.996E.004 23.996E.004 23.96E.004 23.96E.004 23.96E.004 23.96E.004 23.96E.004	2.99E 1.19F 2.19F 2.19F 2.19F 1.006	5.97E-65 0.00E 00 0.00E 00 0.00E 00 0.00E 00 0.00E 00 1.75E-04 1.75E-03 2.25E-03 1.91E-03	5.44E 00.00E 00.	0.006 00 0.006 00 00 00 0006 00 0006 00 0006 00 0006 00 0006 00 0006 00 0006 00 0006	0.00E 00 0.00E 00 0.00E 00 0.00E 00 0.00E 00 0.00E 00 1.19E-04 1.19E-04 1.79E-04 1.79E-04 1.79E-04	0.00E 00 0.00E 00 0.00E 00 5.97E-05 0.00E 00 0.00E 00 1.19E-04 1.19E-04 1.19E-04 1.19E-04	0.00E 00 0.00E 00 0.0	00.00E 00 00.00E
1 APA 77 900 1000 1000 1100 1100 1100 1120 1120 1	4.65c-102 3.63f-102 3.63f-102 3.63f-102 2.76f-102 2.76f-102 1.65f-102 1.64f-102 2.74c+102 2.74c+102 2.74c+102	2.746 2.176 2.176 2.176 2.176 1.996 1.996 1.026 9.016 9.016 9.016 9.016 1.406			2.756-03 2.036-03 2.036-03 2.576-03 1.5916-03 1.5916-03 1.5916-03 1.5916-03 2.3916-03 2.3916-03 2.3916-03	11.45.50		3.5 5 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	1.795-04 2.395-04 2.395-04 0.005-00 1.795-04 0.006-00 0.006-00 1.196-04 1.796-04 1.186-04 4.186-04	2.394-04 5.976-05 11.196-04 11.196-04 5.976-05 5.976-05 6.006 00 0.006 00 0.006 00 0.006 00 1.196-04	5.976-05 1.196-04 1.196-04 5.976-05 0.006 00 0.006 00 0.006 00 0.006 00 0.006 10 1.7976-05
2 APR 77 1700 4 APR 77 930 1030 1030	3.77E-02 4.45E-02 4.88E-02 5.01E-02 7.94c-62	2.46E-72 3.07E-02 3.00E-02 3.13E-02 5.29r-03	1.935-72 2.186-72 2.000-02 3.436-02	7.35E-03 9.97F-03 1.05F-32 1.11E-02	4.016-03 5.616-03 5.556-03 7.226-03 9.436-03	2.126-03 2.806-03 3.646-03 4.296-03 6.086-03	1.37E-03 2.98E-03 2.26E-03 2.93E-03 3.76E-03	8.36E-04 1.49E-03 1.79E-03 2.26E-03	5.37E-04 8.95E-04 1.37E-03 5.97E-04 1.91E-03	3.94E-04 5.37E-04 9.35E-04 1.07E-03	3.58E-04 7.76E-04 7.16E-04 1.25E-03

				YO.	wer Acrosol Stre Distribution Measurements	8	Tapl	0 0	oist.	֓֞֝֟֓֓֓֓֓֓֓֓֟֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֟֓֓֓֓֓	one to	ž	easul	eme	ints				
			Part	102	Particle Density (1/cc/µm) vs. Particle Radius	nsi	ty ()	1/cc	/mm/	>	3. P	arti	cle	Rac	itus	(mn)	ê		
RADIUS>	0.12		0.15	**	0.19	•	0.22		0.26		0.23		0.33		1.22		2-13	3.12	4.07
4 APA 77 LE33 1230 1230 1230 1230 1330 1330 1540 1540 1540 1540 1540 1540 1540 154		MAMMAMAMAMA			4.00 4.00 6.00 6.00 6.00 6.00 6.00 6.00 6.00 1.10	222222222222222222222222222222222222222	2. 186 02 2. 186 02 2. 186 02 2. 186 02 2. 676 02 3. 66 02 3. 68 02 3. 68 02 3. 68 02 3. 68 02	72 72 72 72 72 72 72 72 72 72 72 72 72 7	11.00£ 02 11.40£ 02 11.40£ 02 11.59£ 02 11.59£ 02 11.41£ 02 2.45£ 02 2.45£ 02	2222222222	6.33E 01 8.60E 01 8.60E 01 1.15E 02 1.15E 02 1.15E 02 1.45E 02 1.45E 02 1.45E 02 1.45E 03 1.45E 03 1.45E 03 1.45E 03	11 11 12 22 22 22 22 22 22 22 22 22 22 2	4.176 01 4.526 01 4.526 01 7.276 01 1.006 02 1.006 02 1.006 01 1.006 02 1.006 02		\$5.50 00 \$5.50 00 \$5.53 00 \$5.53 00 \$5.53 00 \$5.44 00 \$5.		1.25E 00 1.25E 00 1.25E 00 1.25E 00 1.35E 00 1.55E 00 1.55E 00 1.55E 00 1.55E 00 1.55E 00 1.55E 00 1.55E 00	3.286-01 2.4606-02 2.4606-02 2.486-03 3.696-03 3.996-03 3.46-03 3.46-03 3.46-03 3.46-03 3.46-03 3.46-03 3.46-03 3.46-03 3.46-03 3.46-03 3.46-03 3.46-03 3.46-03 3.46-03	101 102 100 100 100 100 100 100 100 100
1700 5 APR 77 1000	2.658	5 55	8.86	3 23	7.86E 02	28	3.406 02	27	2.19E 02	200	1.54E 02	202	1.846 02 1.36E 02	222	2.75E	888	2.75E 00 5.44E-01 2.57E 00 4.95E-01 7.19E-01 1.74E-01	1.926-01 1.716-01 4.766-02	5.2%E-02 4.5%E-02 1.31E-02

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Particle Density (1/cc/um) vs. Particle Radius (um)
NRL Aerosol Size Distribution Measurements
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ACKNOWLEDGEMENTS

The programmatic support provided by Dr. D. Finkleman and Lt. M. Hughes, Naval Sea Systems Command, PM-22/PMS-405 is gratefully acknowledged. Support by the Naval Ordnance Test Unit (NOTU) and the Air Force Eastern Test Range (AFETR), Patrick AFB, Florida in making available the CCAFS sites for use in this program is greatly appreciated. In particular, many thanks are due to NOTU personnel, Ms. H. Cassidy, D. Burdett, L. LaMarre, D. Walker, and R. Woehle for their help. The continuing field support of the NRL program by the Facilities and Cape Operations Office of NOTU under E. Knott is responsible, in large measure, for the success of the work reported here. In this regard it is a pleasure to acknowledge the assistance provided by H. Brekemridge, Ms. C. Riddle, and R. Williamson. The day to day assistance and communication cheerfully offered by Mr. Williamson contributed immeasurably to the efficient performance of the NRL program.

Technical assistance provided by F. Tidball is greatly appreciated. Excellent machine work and logistical support were provided by M. Woytko. The authors wish to thank C. Acton and Mrs. J. Pinkney for their assistance in the preparation of this report.